

March 3, 2023

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Re: Geotechnical Report Proposed Manufacturing Building Cranston, Rhode Island LGCI Project No. 2252-Rev. 1

Dear Mr. Giampietro:

Lahlaf Geotechnical Consulting, Inc. (LGCI) has completed a geotechnical study for the proposed Manufacturing Building in Cranston, Rhode Island. We are submitting our geotechnical report electronically.

The soil and rock samples from our explorations are currently stored at LGCI for further analysis, if requested. Unless notified otherwise, we will dispose of the soil and rock samples after three (3) months.

Thank you for choosing LGCI as your geotechnical engineer.

Very truly yours,

Lahlaf Geotechnical Consulting, Inc.

in

Abdelmadjid M. Lahlaf, Ph.D., P.E. Principal Engineer



GEOTECHNICAL REPORT PROPOSED MANUFACTURING BUILDING CRANSTON, RHODE ISLAND

LGCI Project No. 2252-Rev. 1 March 3, 2023

Prepared for:

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GEOTECHNICAL REPORT PROPOSED MANUFACTURING BUILDING CRANSTON, RHODE ISLAND LGCI Project No. 2252-Rev. 1

March 3, 2023

Prepared for:

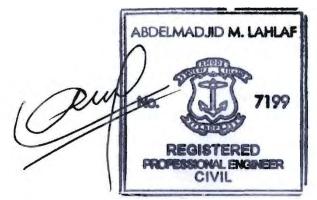
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Prepared by:

LAHLAF GEOTECHNICAL CONSULTING, INC.

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Abdelmadjid M. Lahlaf, Ph.D., P.E. Principal Engineer

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Figure 2	Surficial Geologic Map
Figure 3	Exploration Location Plan

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Appendix A	LGCI's Test Pit Logs
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Appendix C	Laboratory Test Results

Geotechnical Report Proposed Manufacturing Building Cranston, Rhode Island LGCI Project No. 2252-Rev. 1

1. PROJECT INFORMATION

1.1 Project Authorization

This geotechnical report presents the results of the subsurface explorations and a geotechnical evaluation performed by Lahlaf Geotechnical Consulting, Inc. (LGCI) for the proposed Manufacturing Building in Cranston, Rhode Island. To date, we have performed our services in two phases as follows.

We performed our original services in general accordance with our proposal No. 22037-Rev. 1 dated September 7, 2022, revised on September 19, 2022. Mr. Jon Giampietro of Taco Comfort Solutions (TCS) authorized our original services by signing our proposal on October 9, 2022.

We performed additional services in general accordance with our proposed No. 23012 dated February 9, 2023. Mr. Jon Giampietro of TCS authorized our additional services by signing our proposal on February 13, 2023.

1.2 Purpose and Scope of Services

The purpose of our geotechnical services was to perform subsurface explorations at the site for the proposed manufacturing building, and to provide foundation design and construction recommendations. LGCI performed the following services:

- Coordinated our exploration locations with TCS and with Mr. Robert Kelliher of Thermo-Mechanical Systems Corporation (TMSC), the project manager.
- Marked the exploration locations at the site and notified Dig Safe Systems Inc. (Dig Safe) and the City of Cranston for utility clearance.
- Engaged a drilling subcontractor for a total of six (6) days to advance nineteen (19) soil borings at the site, including four (4) days to advance seventeen (17) soil borings as part of our original services and two (2) days to advance an additional two (2) soil borings as part of our additional services.
- Observed fifteen (15) test pits performed at the site by an excavator subcontractor hired by TMSC.
- Provided an LGCI geotechnical engineer at the site to coordinate and observe the test pits and borings, describe the soil samples, and prepare field logs.
- Submitted fourteen (14) soil samples from the test pits for laboratory testing, including four (4) samples included in our scope, six (6) additional samples approved by the owner as part of our original services, and four (4) samples as part of our additional services. The laboratory tests included eight (8) grain size analyses, two (2) organic content tests on fill from



explorations performed as part of our original services, and four (4) organic content tests on buried organic soil from our additional service explorations.

• Prepared this geotechnical report containing the results of our subsurface explorations and our recommendations for foundation design and construction.

Upon the completion of our original services, LGCI submitted a geotechnical report dated January 16, 2023. This geotechnical report includes the results of our original services and supersedes the aforementioned report.

Our scope does not include preparing specifications, reviewing contract documents, attending meetings, or providing construction services. LGCI would be pleased to perform these services when needed. Recommendations for unsupported slopes, stormwater management, erosion control, pavement design, slope stability analyses, liquefaction and/or site-specific seismic analysis, pile analysis and design, and cost or quantity estimates are not included in our scope of work.

LGCI's scope of services does not include an environmental assessment for the presence or absence of wetlands or analytical testing for hazardous or toxic materials in the soil, surface water, groundwater, or air, on or below or around this site, or mold in the soil or in any structure at the site. Any statements regarding odors, colors, or unusual or suspicious items or conditions are strictly for the information of the client.

1.3 Site Description

Our understanding of the site is based on our field observations, our discussions with TMSC, and on the following documents:

- Document titled: "Environmental Land Usage Restriction," (ELUR Document) dated January 19, 2015, and provided to LGCI by TMSC via e-mail on March 21, 2022.
- Drawing C-200 titled: "Civil Proposed Site Plan, Taco, Inc., 1160 Cranston Street, Cranston, RI 02920, 35 Carlsbad Building," (Site Plan) prepared by Woodard & Curran, dated August 2022, and provided to LGCI by TMSC via email on August 23, 2022.
- Drawing titled: "Exiting Conditions, Assessors Plat 7-3, Lots 3141 & 3744, 35 Carlsbad Street, Cranston, RI 02920," (Existing Conditions Plan), prepared by Crossman Engineering, dated April 5, 2022, and provided to LGCI by TMSC on August 23, 2022.

The site is located east of the existing TCS building located at 1160 Cranston Street in Cranston, Rhode Island as shown in Figure 1. The site is bordered by Carlsbad Street on the western side, by Burnham Street on the southern side, by Carolina Street on the northern side, and by Washington Secondary Trail on the eastern side. The site is currently used as a parking lot and tractor trailer storage yard. The site consists of asphalt and concrete parking areas and grass

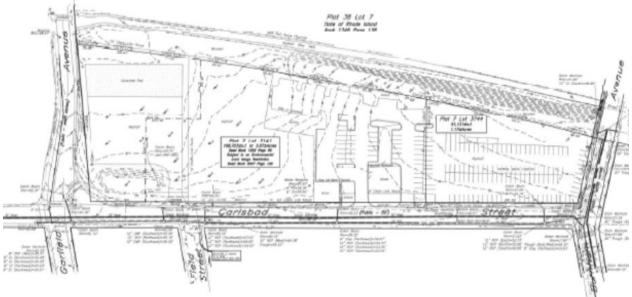


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landscape features. A portion of the site is capped with crushed stone and geotextile fabric due to an Environmental Land Usage Restriction (EULR) described below.

Based on the Site Plan, the grades at the site generally range from El. 52 feet near Burnham Street near the southeastern corner of the site and El. 70 feet near Carolina Street near the northeastern corner of the site. The existing grades within the general area of the proposed building (described in Section 1.4) range between El. 57 feet near the southern side of the proposed building and El. 68 feet near the northern side of the proposed building. The existing grades within the general area of the proposed northern parking lot range between El. 62 feet and El. 69 feet. The existing grades within the general area of the proposed southern parking lot range between El. 54 feet and El. 59 feet.

Based on the Existing Conditions Plan, the site is divided into two (2) lots as shown in the plan below: a northern Lot 3141 zoned C-4 on the northern side and M-2 on the southern side, and a southern Lot 3744 zoned M-2. Lot 3141 comprises most of the site and has an area of about 3.87 acres. Lot 3744 has an area of about 1.17 acres.



Excerpt from Existing Conditions Plan

We understand that the northern portion of the site, i.e., Lot 3141, has an EULR. Based on the ELUR Document, we understand that the site is capped and that the top several feet of soil consist of contaminated soil. We understand that as a result of the ELUR on Lot 3141, materials excavated from the northern portion of the site, i.e., Lot 3141, cannot be transferred or reused on the southern side in Lot 3744.

1.4 Project Description

Our understanding of the proposed construction is based on our discussions with TMSC and the documents listed in Section 1.3.



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We understand that TCS is planning to develop the site into a new manufacturing building. We understand that the proposed construction will consist of a one-story manufacturing building located on the northern side of the site that will have a footprint of about 85,500 square feet. The proposed building will be located entirely in Lot 3141. We understand that the proposed building will not have a basement.

We understand that the proposed grading, including the finished floor elevation of the proposed building, is a work in progress and will be finalized based on the results of this report and on the environmental constraints from the ELUR. The grading information described herein is preliminary and is based on the drawings listed in Section 1.3.

Based on the Site Plan, the proposed building will have a first finished floor elevation (FFE) of El. 64 feet; thus, requiring cuts of up to 4 feet on the northern side and fills of up to 7 feet on the southern side to achieve the proposed grade of the building.

We understand that the proposed construction will also consist of paved parking lots located to the north and south of the proposed building. The proposed grades within the proposed northern parking lot will range between El. 62 feet and El. 68 feet, requiring cuts of about 2 feet and fills of about 2.5 feet to achieve the proposed grades. The proposed grades within the proposed southern parking lot will range between El. 56 feet and El. 62 feet, requiring fills ranging between 2 and 6 feet to achieve the proposed grades. The northern parking lot will be accessible from Carolina Street via an access road. The southern parking lot will be accessible from Burnham Street via an access road.

We understand that after the proposed grades are finalized, the magnitude of the cuts and fill described above may change slightly. However, the general pattern of the earthwork operation will still remain as consisting of slights cuts on the northern side and fill on the southern side of the site.

1.5 Elevation Datum

We understand that the elevations provided in the Site Plan and Existing Conditions Plan are referenced with respect to the North American Vertical Datum of 1988 (NAVD88). Elevations are in feet.



2. SITE AND SUBSURFACE CONDITIONS

2.1 Surficial Geology

LGCI reviewed a surficial geologic map titled: "Geologic Map of Providence Quadrangle, Rhode Island, Surficial Geology," prepared by J. Hiram Smith in 1956, Geological Survey, Map GQ-84.

The surficial geologic map of the site indicates that the natural soils in the general vicinity of the site consist of outwash plains.

The outwash plains consist of sorted sand and local deposits of coarse gravel.

The Surficial Geologic Map is shown in Figure 2.

2.2 LGCI's Explorations

2.2.1 General

LGCI coordinated our exploration locations with TMSC and marked the exploration locations in the field. LGCI notified Dig Safe and the City of Cranston for utility clearance prior to starting our explorations at the site.

Unless notified otherwise, we will dispose of the soil and rock samples obtained during our explorations after three (3) months.

2.2.2 LGCI's Test Pits

LGCI observed fifteen (15) test pits (TP-1 to TP-15) excavated at the site by JRD, Inc. of Assonet, Massachusetts on November 14 and 15, 2022. The test pits were excavated using a Deere 710G backhoe. The test pits extended to depths ranging between 9 feet and 12 feet beneath the ground surface. Upon completion, the test pits were backfilled with the excavated material in 12-inch to 18-inch lifts and tamped with the excavator bucket.

An LGCI geotechnical engineer observed and logged the test pits in the field.

2.2.3 LGCI's Soil Borings

As part of our original services, LGCI engaged Northern Drilling Services, Inc. (NDS) of Northborough, Massachusetts to advance seventeen (17) soil borings (B-1 to B-17) at the site between December 19 and 22, 2022. The borings were advanced with a Mobile B-53 ATV Drill Rig using 3 ¹/₄" inner diameter hollow stem augers. The borings extended to depths ranging between 12 and 22 feet beneath the ground surface. Upon completion, the boreholes were backfilled with the soil cuttings and sand. The ground surface was restored with asphalt cold patch in paved areas.



During our additional services, LGCI engaged NDS to advance an additional two (2) soil borings (B-101 & B-102) at the site on February 17 and 20, 2023. The borings were advanced with a Mobile B-48 ATV Drill Rig using drive and wash boring techniques with 4-inch casings. Borings B-101 and B-102 extended to depths ranging between 49 and 53.5 feet beneath the ground surface, respectively. Upon completion, the boreholes were backfilled with the soil cuttings and gravel. The ground surface was restored with asphalt cold patch.

NDS performed Standard Penetration Tests (SPT) and obtained split spoon samples with an automatic hammer at typical depth intervals of 2 feet or 5 feet as noted on the boring logs in general accordance with ASTM D-1586.

An LGCI geotechnical engineer observed and logged the borings in the field.

2.2.4 Exploration Logs and Locations

The boring and test pit locations are shown in Figure 3. Appendix A contains LGCI's test pit logs. Appendix B contains LGCI's boring logs. Tables 1 and 2 include summaries of LGCI's test pits and borings, respectively.

2.3 Subsurface Conditions

The subsurface description in this report is based on a limited number of explorations and is intended to highlight the major soil strata encountered during our explorations. The subsurface conditions are known only at the actual exploration locations. Variations may occur and should be expected between exploration locations. The boring and test pit logs represent conditions that we observed at the time of our explorations and were edited, as appropriate, based on the results of the laboratory test data and inspection of the soil samples in the laboratory. The strata boundaries shown in our boring and test pit logs are based on our interpretations and the actual transitions may be gradual. Graphic soil symbols are for illustration only.

The soil strata encountered in LGCI's test pits and borings were as follows, starting at the ground surface.

<u>Asphalt</u> – Asphalt was encountered at the ground surface in test pits TP-1 to TP-4, TP-11, and TP-13 and in borings B-1 to B-6, B-12, B-14 to B-16, B-101, and B-102. The thickness of the asphalt ranged between 0.2 feet and 0.4 feet.

<u>Topsoil</u> – A layer of surficial organic topsoil was encountered at the ground surface in test pits TP-5 to TP-7, TP-10, and TP-12, and in borings B-7 and B-13. The thickness of the topsoil ranged between 0.2 feet and 2 feet beneath the ground surface.

<u>Crushed Stone</u> – A layer of crushed stone was encountered at the ground surface in test pits TP-8 to TP-9, and TP-14 to TP-15, and in borings B-8 to B-11, and B-17. The thickness of the crushed stone ranged between 0.3 feet and 0.5 feet.



<u>Fill</u> – A layer of fill was encountered beneath the asphalt, topsoil, or crushed stone in all test pits and borings, except in test pit TP-7. The fill extended to depths ranging between 1 foot and 12 feet beneath the ground surface. The samples in this layer were mostly described as silty sand, well graded sand, or poorly graded sand. Two (2) samples were described as well graded gravel. The fines content in the fill ranged between 0 and 30 percent, but was in most samples less than 20 percent. The gravel content in the fill ranged between 0 and 30 percent. When described as gravel, the sand content in the fill ranged between 15 and 30 percent. The fill contained traces of organic soil, brick, roots, concrete, asphalt, wood, plastic, glass, clay pipe, and construction debris.

The SPT N-values in this layer ranged between 3 blows per foot (bpf) and 54 bpf, with most values ranging below 15 bpf, indicating very loose to medium dense material. Please note that the high SPT N-values recorded in the fill may be due to obstructions such as cobbles and boulders present in the fill and may not represent the true density of the fill. Also, the deeper fill was generally looser than the shallow fill. The excavation effort in the fill layer was described as easy to moderate.

<u>Buried Organic Soil</u> – A layer of buried organic soil was encountered beneath the fill in test pits TP-4 and TP-6, and in borings B-2, B-4, and B-102 performed within or near the southern side of the proposed building. The buried organic soil extended to depths ranging between 8 feet and 11 feet beneath the ground surface. The samples in this layer were described as silty sand. The fines content in the buried organic soil ranged between 20 and 35 percent and the gravel content ranged between 5 and 10 percent. The buried organic soil contained traces of organic soil and roots.

The SPT N-values in this layer ranged between 2 and 10 bpf, indicating very loose to loose material. The excavation effort within this layer was described as easy.

<u>Buried Subsoil</u> – A layer of buried subsoil was encountered beneath the fill in test pits TP-1, TP-3, and TP-5. The buried subsoil extended to depths ranging between 5 feet and 7.7 feet beneath the ground surface. The samples in this layer were described as silty sand and well graded sand. The fines content in the buried subsoil ranged between 10 and 20 percent and the gravel content ranged between 15 and 20 percent. The buried subsoil contained traces of organic soil and roots.

The excavation effort within this layer was described as easy, indicating loose material.

<u>Sand and Gravel</u> – A layer of sand and gravel was encountered beneath the topsoil, fill, buried organic soil, or buried subsoil in all test pits and borings. The sand and gravel extended to the termination depths of the test pits and borings, except in borings B-101 and B-102 where the sand and gravel extended to depths of 33 feet and 44 feet beneath the ground surface, respectively. The samples in this layer were mostly described as poorly graded sand and well graded sand. Five (5) samples were described as silt, three (3) samples were described as silty sand, and two (2) samples were described as well graded gravel. The fines content in this layer ranged between 0 and 40 percent, with most samples containing less than 25 percent fines. The gravel content ranged between 0 and 35 percent. When described as gravel or silt, the sand



content in this layer ranged between 20 and 45 percent. The silt was described as non-plastic. One (1) sample within this layer contained traces of weathered rock.

The SPT N-values in this layer ranged between 3 bpf and 66 bpf, with most values ranging between 10 bpf and 31 bpf, indicating mostly medium dense material. Please note that the high SPT N-values recorded in the sand and gravel may be due to obstructions such as cobbles and boulders present in the sand and gravel and may not represent the true density of the sand and gravel.

<u>Silt</u> – A layer of silt was encountered beneath the sand and gravel in boring B-101 and within the sand and gravel layer in boring B-102. The silt extended to depths of 45 feet and 39 feet beneath the ground surface in borings B-101 and B-102, respectively. The samples within this layer were described as silt with sand. The sand content within this layer ranged between 10 and 20 percent. The silt was described as non-plastic to moderately plastic. A few samples within this layer contained traces of weathered rock.

The SPT N-values in this layer ranged between 3 bpf and 12 bpf, indicating soft to medium stiff silt. Split spoon refusal was encountered on apparent rock within this layer in boring B-101 at a depth of 45 feet beneath the ground surface.

<u>Weathered Rock</u> – A layer of weathered rock was encountered beneath the sand and gravel in boring B-102 at a depth of 44 feet beneath the ground surface. The weathered rock extended to a depth of 46 feet beneath the ground surface. The sample within this layer was described as silty sand. The fines content within this layer ranged between 20 and 25 percent and the gravel content ranged between 20 and 25 percent.

Split spoon refusal was encountered on rock within this layer at a depth of 46 feet beneath the ground surface.

 $\underline{\text{Rock}}$ – Split spoon refusals were encountered in borings B-101 and B-102 at depths of 45 feet and 46 feet beneath the ground surface, respectively.

To confirm and characterize the rock, rock was cored in boring B-101. The rock consisted of a very soft to soft, fresh, moderately fractured to sound, black, fine-grained, Shale. The rock core recovery was 100 percent, and the Rock Quality Designation (RQD) was 56.7 percent. The coring rate ranged between 2.0 and 4.0 minutes per foot (min./ft.).

2.4 Groundwater

Groundwater was encountered in test pits TP-1 to TP-5, and in all borings except in borings B-1 and B-11 at depths ranging between 6.0 and 22.0 feet beneath the ground surface, as shown in Tables 1 and 2 and in the boring and test pit logs.

The groundwater information reported herein is based on observations made during or shortly after the completion of drilling or excavation. In addition, water was introduced into borings B-



101 and B-102 during drilling. Therefore, the reported groundwater levels may not represent the actual groundwater conditions, as additional time may be required for the groundwater levels to stabilize. The groundwater information presented in this report only represents the conditions encountered at the time and location of the explorations. Seasonal fluctuation should be anticipated.

2.5 Laboratory Test Data

LGCI submitted eight (8) soil samples collected from the test pits for grain-size analysis. The results of the grain-size analyses are provided in the test data sheets included in Appendix C and are summarized in the table below.

Test Pit No.	Sample No.	Stratum	Sample Depth (ft.)	Percent Gravel	Percent Sand	Percent Fines
TP-4	Grab	Fill	0.3 - 3.0	31.6	56.8	11.6
TP-5	Grab	Silt	7.7 - 12.0	0.1	40.1	59.8
TP-6	Grab	Fill	1.5 - 8.5	32.6	55.5	11.9
TP-7	Grab	Sand and Gravel	2.0 - 5.0	25.5	72.7	1.8
TP-8	Grab	Fill	0.3 - 5.5	29.4	56.4	14.2
TP-9	Grab	Fill	0.3 - 5.0	49.4	42.1	8.5
TP-10	Grab	Fill	0.8 - 6.5	17.3	76.6	6.1
TP-15	Grab	Fill	0.3 - 4.0	46.4	49.2	4.4

Grain-Size Analysis Test Results

LGCI also submitted two (2) soil samples from the fill strata in test pits TP-3 (from 0.5 feet to 4 feet) and TP-13 (from 0.5 feet to 5 feet) to a laboratory for organic content tests, and the tests indicated organic contents (by weight) of 2.6 and 2.2 percent, respectively. LGCI also submitted four (4) soil samples from the buried organic soil stratum in the borings B-2 (from 8 feet to 10 feet), B-4 (from 6 feet to 8 feet), and B-102 (from 8 feet to 10 feet), and from test pit TP-4 (from 6.5 to 9.0 feet). The results from these tests will be provided separately.



3. EVALUATION AND RECOMMENDATIONS

3.1 General

Based on our understanding of the proposed construction, our observation of our borings, and the results of our laboratory testing, there are a few issues that we would like to highlight for consideration and discussion.

3.1.1 Asphalt, Surficial Topsoil, Existing Fill, Buried Topsoil, and Buried Subsoil

- Asphalt, topsoil, existing fill, crushed stone cap, buried topsoil, and buried subsoil were encountered in the borings. These materials are not suitable to support foundations.
- The asphalt and the surficial topsoil should be removed from within the entire construction area, including the proposed building footprint and the proposed driveways and parking lots.
- The existing fill was observed to be variable in composition and was generally very loose to medium dense. In addition, variable amounts of organic matter were noted in several of the fill samples. Existing fill that was not placed with strict moisture, density, and gradation control presents risk of unpredictable settlement that may result in poor performance of floor slabs and foundations. Due to these risks, the existing fill as well as the buried topsoil and buried subsoil should be entirely removed from within the proposed building footprint. We anticipate that the removal will extend up to depths of about 12 feet. The removal may extend to greater depths at locations not explored by LGCI. Laterally, the removal should extend beyond the proposed building footprint a distance equal to the distance between the bottom of the proposed footings and the top of the natural sand and gravel, or 5 feet, whichever is greater.
- We recommend segregating the buried organic topsoil and buried subsoil from the existing fill. After the excavation of the existing fill and the buried organic topsoil and buried subsoil is completed, the existing fill may be placed back in 9-inch loose lifts and compacted to 95 percent relative compaction. Whereas the existing fill generally contained a fines content higher than 10 percent, we recommend improving the existing fill to meet the gradation of Structural Fill by blending it with crushed stone and use the blend under footings and within 3 feet from the bottom of the proposed slab. We estimate that a blending ratio of about 2 parts crushed stone to 5 parts existing fill would produce a blend that meets the gradation requirements for Structural Fill. The blending ratios may be revised during construction based on grain-size analyses on bulk samples. The Structural Fill should extend to within the zone of influence of footings, i.e., within a zone defined by a line inclined at 45 degrees and extending from the outside edge of the proposed footing downward and outward.



- The blending of the existing fill with crushed stone will generate surplus material, mainly of existing fill. The surplus material could be reused to raise the grades at the site including in the southern lot (Lot 3744). This would require combining the two lots and applying, if possible, the ELUR on the combined lot. If this is not possible, a cost benefit analysis should be performed to compare the cost of the excavation, blending, replacement, and disposal of the surplus material to another option such as ground improvements by means of aggregate piers as described later in this report.
- The subgrade of footings should be prepared in accordance with the recommendations in Section 4.1.
- Within paved areas, the existing fill, should be removed to the top of the natural sand and gravel or to a depth of 18 inches beneath the bottom of the proposed pavement. Where organic soil is exposed, the organic soil should be removed. Where existing fill or buried subsoil are exposed, the existing fill deeper than 18 inches beneath the bottom of the proposed pavement can remain in place provided that it is firm and unyielding following proofrolling and compaction as described in Section 4.1.

3.1.2 Aggregate Piers

Aggregate piers (APs) are typically relatively short, stiff elements of compacted aggregate which improve the existing fill. These elements are typically installed by augering holes ranging from 20 inches to 36 inches in diameter. Aggregate (new crushed stone, recycled concrete, or other granular material) is then introduced into the hole and is generally compacted in one-foot lifts by repeated penetrations with the vibrator, which can be mounted to a crane or tracked carrier. The vibratory or ramming energy densifies the aggregate in the element; thus, producing high modulus aggregate piers. The installation of APs also densifies the surrounding soil depending on the type of soil. These high modulus elements reinforce the treatment zone and increase the composite friction angle and stiffness of the reinforced soil mass. The design of APs is typically verified with a modulus load test.

Where the subsurface conditions include a layer of organic soil and/or peat, the aggregate piers should be grouted in order to reduce the potential for bulging of the AP elements in the soft organic material or peat.

The work of the specialty contractor installing the APs should be coordinated with that of the site contractor who should perform pre-trenching for possible boulders, abandoned foundations, metal pipes, or other obstructions before the installation of the APs.

While the AP installation generates little spoils. Where it is not desired to generate spoils during the improvement process, vertical displacement APs could be used. These are installed by driving a mandrel and hammer to the design depth, feeding the backfill material through the hollow mandrel, and compacting the backfill in one-foot lifts using the hammer; thus, generating no spoils. Vertical displacement APs are typically installed with diameters



ranging between 12 and 16 inches to typical depths ranging between 15 and 35 feet, and to depths of up to 60 feet where needed.

The length of the APs should be based on improvements that reduce the total and differential settlement to within the thresholds established for the project for both static and earthquake loads.

To reduce the length of the APs, we believe that the APs should be installed from the current grade, before placing the Structural Fill required to raise the grades. This option will result in shorter APs under the proposed slab. However, this option will likely require more AP elements under the proposed slab.

The ground improvement technologies are patented, and the design is performed by the specialty contractors. We recommend that if the ground improvement option is selected, the project plans and specifications for ground improvement be performance-based, allowing a variety of ground improvement contractors the opportunity to bid the work. Specifications should indicate the required allowable bearing pressure for footings and slabs, and the allowable total and differential settlements for the structure, including static and earthquake induced settlement. In addition, we recommend that the specifications require that the supporting design calculations be available for review by the design team. Ground improvement contractors should also be provided with grading plans and subsurface information associated with the proposed structure for use in preparing their bids.

3.1.3 Shallow Foundations

Based on the results of the borings, the subsurface conditions are suitable to support shallow spread and continuous footings bearing on Structural Fill placed directly on top of the sand and gravel layer after entirely removing the asphalt, the existing fill, the buried topsoil, and the buried subsoil, or on ground improved with aggregate piers. Our recommendation for net allowable bearing capacity in the sand and gravel is presented in Section 3.2.1.

3.2 Foundation Recommendations

3.2.1 Footing Design

- We recommend entirely removing the surficial topsoil, buried organic soil, buried subsoil, and the existing fill from within the proposed building footprint or improving the site with APs as described in Section 3.1.
- We recommend supporting the proposed building on spread footings bearing on Structural Fill placed directly on the natural sand and gravel or on ground improved with APs.
- We recommend designing the proposed footings using a net allowable bearing pressure of 4 kips per square foot (ksf). We recommend that the footings bear on a minimum of 12 inches of Structural Fill placed directly on top of the natural sand or on ground improved



with APs. The Structural Fill should extend at least on foot laterally beyond the limits of the footings.

- Footing subgrades should be prepared in accordance with the recommendations in Section 4.1.
- All foundations should be designed in accordance with *The Rhode Island State Building Code* (RISBC).
- Exterior footings and footings in unheated areas should be placed at a minimum depth of 4.5 feet below the final exterior grade to provide adequate frost protection. Interior footings in heated areas may be designed and constructed at a minimum depth of 2 feet below finished floor grades.
- Wall footings should be designed and constructed with continuous, longitudinal steel reinforcement for greater bending strength to span across small areas of loose or soft soils that may go undetected during construction.
- A representative of LGCI should be engaged to observe that the subgrade has been prepared in accordance with our recommendations.

3.2.2 Settlement Estimates

Based on our experience with similar soils and designs using a net allowable bearing pressure of 4 ksf, we anticipate that the total settlement will be approximately 1 inch, and that the differential settlement of the footings will be 3/4 inch or less over a distance of 25 feet. We believe that total and differential settlements of this magnitude are tolerable for a similar structure. However, the tolerance of the proposed structure to the predicted total and differential settlements should be assessed by the structural engineer.

If the site is improved using APs, the specialty contractor should design the APs to limit the settlement within the limits listed above.

3.3 Concrete Slab Considerations

3.3.1 Slabs-on-Grade

• Floor slabs should be constructed as a slabs-on-grade bearing on a minimum of 12 inches of Structural Fill placed directly on top of the natural sand and gravel or on top of ground improved with APs. The subgrade of the slabs should be prepared as described in Section 4.1.



- To reduce the potential for dampness in the proposed floor slab, the project architect may consider placing a vapor barrier beneath the floor slab. The vapor barrier should be protected from puncture during the placement of the proposed slab reinforcement.
- For the design of the floor slab bearing on the materials described above, we recommend using a modulus of subgrade reaction, k_{s1}, of 80 tons per cubic foot (tcf). Please note that the values of k_{s1} are for a 1 x 1 square foot area. These values should be adjusted for larger areas using the following expression:

Modulus of Subgrade Reaction
$$(k_s) = k_{s1} * \left(\frac{B+1}{2B}\right)^2$$

where:

- k_s = Coefficient of vertical subgrade reaction for loaded area;
- k_{s1} = Coefficient of vertical subgrade reaction for a 1 x 1 square foot area; and
- B = Width of area loaded, in feet.

Please note that cracking of slabs-on-grade can occur as a result of heaving or compression of the underlying soil, but also as a result of concrete curing stresses. To reduce the potential for cracking, the precautions listed below should be closely followed during the construction of all slabs-on-grade:

- Construction joints should be provided between the floor slab and the walls and columns in accordance with the American Concrete Institute (ACI) requirements, or other applicable code.
- The backfill in interior utility trenches should be properly compacted.
- In order for the movement of exterior slabs not to be transmitted to foundations or superstructures, exterior slabs, such as approach slabs and sidewalks, should be isolated from the superstructure.

3.3.2 Under-slab Drains and Waterproofing

Based on the groundwater level observed in the borings, we believe that an under-slab drainage system is not required.

If the proposed building includes an elevator pit or other structure that extends beneath the FFE, such elevator pit or other structure should be designed to be waterproof.



3.4 Seismic Design

Based on the SPT N-values from the borings, we estimate that the seismic criteria for the site are as follows:

•	Site Class:	D
٠	Spectral Response Acceleration at short period (Ss):	0.178g
•	Spectral Response Acceleration at 1 sec. (S1):	0.063g
•	Site Coefficient Fa (Table 1613.5.3(1)):	1.6
•	Site Coefficient Fv (Table 1613.5.3(2):	2.4
•	Adjusted spectral response S _{MS} :	0.285g
•	Adjusted spectral response S _{M1} :	0.151g

A few low SPT N-values were recorded in borings B-4, B-5, and B-6 advanced on the southern side of the proposed building as part of our explorations performed as part of our original services. To explore whether low SPTs are present deeper than the bottom of the explorations performed as part of our original services, additional borings B-101 and B-102 were advanced to the top of rock. Borings B-101 and B-102 indicated that the low SPT N-values recorded in borings B-4, B-5, and B-6 were isolated, i.e., they were not indicative of a distinct, loose sublayer within the sand and gravel layer. Accordingly, and based on the SPT N-value data from the borings, the site soils are not susceptible to liquefaction.

3.5 Lateral Pressures for Wall Design

3.5.1 Lateral Earth Pressures

Lateral earth pressures for the design of below-grade walls, if any, and site retaining walls are provided below.

Coefficient of Active Earth Pressure, KA:	0.31	
Coefficient of At-Rest Earth Pressure, Ko:	0.47	
Coefficient of Passive Earth Pressure, K _p :	3.3	
Total Unit Weight γ:	125 pcf	

<u>Note</u>: The values in the table are based on a friction angle for the backfill of 32 degrees and neglecting friction between the backfill and the wall. The design active and passive coefficients are based on horizontal surfaces (non-sloping backfill) on both the active and passive sides, and on a vertical wall face.

- Exterior walls of below-ground spaces and other retaining walls braced at the top to restrain movement/rotation, should be designed using the "at-rest" pressure coefficient.
- We recommend placing free-draining material within the 3 feet immediately behind retaining walls.
- We recommend providing weep holes at the bottom of site retaining walls, including temporary SOE systems, to promote drainage where possible. Alternatively, a pipe should



be placed at the base of the wall to collect the water. Groundwater collected by the wall drains should be discharged into a lower area if gravity flow is possible.

- Passive earth pressures should only be used at the toe of the wall where special measures or provisions are taken to prevent the disturbance or future removal of the soil on the passive side of the wall, or in areas where the wall design includes a key. In any case, the passive pressures should be neglected in the top 4 feet.
- Where a permanent vertical uniform load will be applied to the active side immediately adjacent to the wall, a horizontal surcharge load equal to half of the uniform vertical load should be applied over the height of the wall. At a minimum, a temporary lateral construction surcharge load of 100 pounds per square foot (psf) should be applied uniformly over the height of the wall.
- We recommend using an ultimate friction factor of 0.5 between the natural sand and gravel or Structural Fill and the bottom of the wall. Below-grade walls should be designed for minimum factors of safety of 1.5 for sliding and 2.0 for overturning.
- The design of retaining walls should include the seismic increment to the lateral earth pressures.

3.5.2 Perimeter Drains

- We recommend that free-draining material be placed within 3 feet of the exterior of walls of below-ground spaces, if any. To reduce the potential for dampness in below-ground spaces, proposed below-ground walls should be damp-proofed.
- We recommend that drains be provided behind the exterior of walls of below-ground spaces. The drains should consist of 4-inch perforated PVC pipes installed with the slots facing down. Perimeter drains should be installed at the bottom of the wall in 18 inches of crushed stone wrapped in a geotextile for separation and filtration.

To the extent possible, groundwater collected by the wall drains should be discharged in a lower area if gravity flow is possible. In any case, the groundwater collected by the wall drains should be discharged in accordance with municipal, state, and other applicable standards.

3.6 Parking Lots, Driveways, and Sidewalks

3.6.1 General

The subsurface conditions encountered at the site are generally suitable to support the proposed driveways, parking lots, and sidewalks after preparation of the subgrade as described in Section 4.1.



- We recommend entirely removing the existing asphalt and the surficial topsoil from within the footprint of the proposed driveways and parking lots.
- The existing fill should be improved in accordance with the recommendations in Section 4.1.
- Cobbles and boulders should be removed to at least 18 inches below the bottom of the pavement.

3.6.2 Sidewalks

- Sidewalks should be placed on a minimum of 12 inches of Structural Fill with less than 5 percent fines.
- To reduce the potential for heave caused by surface water penetrating under the sidewalk, the joints between sidewalk concrete sections should be sealed with a waterproof compound. The sidewalks should be sloped away from the building or other vertical surfaces to promote flow of water. To the extent possible, roof leaders should not discharge onto sidewalk surfaces.

3.6.3 Pavement Sections

A typical, minimum, standard-duty pavement section that could be used for parking areas is as follows:

- 1.5" Asphalt "Top Course"
- 2.0" Asphalt "Base Course"
- 8" Aggregate Base (Gravel Borrow, RIDOT M.01.09; Table 1, Column 1)

A typical, minimum, heavy-duty pavement section that could be used in access roads and for areas of heavy traffic is as follows:

- 2.0" Asphalt "Top Course"
- 2.5" Asphalt "Base Course"
- 12" Aggregate Base (Gravel Borrow, RIDOT M.01.09; Table 1, Column 1)

The pavement sections shown above represent minimum thicknesses representative of typical local construction practices for similar use. Periodic maintenance should be anticipated.

Pavement material types and construction procedures should conform to specifications of the Rhode Island Department of Transportation, Standard Specifications for Road and Bridge Construction, 2004 Edition with the latest amendment.



Areas to receive relatively highly concentrated, sustained loads such as dumpsters, loading areas, and storage bins are typically installed over a rigid pavement section to distribute concentrated loads and reduce the possibility of high stress concentrations on the subgrade. Typical rigid pavement sections consist of 6 inches of concrete placed over a minimum of 12 inches of subbase material.

3.7 Underground Utilities

Boulders at the bottom of utility trenches should be removed to at least 12 inches below the pipe invert and the resulting excavation should be backfilled with suitable backfill. Utilities should be placed on suitable bedding material in accordance with the manufacturer's recommendations. "Cushion" material should be placed, by hand, above the utility pipe in maximum 6-inch lifts. The lift should be compacted by hand to avoid damage to the utility. Where the bedding/cushion material consists of crushed stone, it should be wrapped in a geotextile fabric.

Compaction of fill in utility trenches should be in accordance with our recommendations in Section 4.3. To reduce the potential for damage to utilities, placement and compaction of fill immediately above the utilities should be performed in accordance with the manufacturer's recommendations.



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4. CONSTRUCTION CONSIDERATIONS

4.1 Subgrade Preparation

- Organic materials, existing fill, buried organic soil, buried subsoil, abandoned utilities, buried foundations, and other below-ground structures should be entirely removed from within the footprint of the proposed building and site structures, including site retaining walls, and exterior stairs, if any, before the start of foundation work. The excavation should be restored with Structural Fill. Alternatively, the ground should be improved with APs.
- Tree stumps, root balls, and roots larger than ½ inch in diameter should be removed and the cavities filled with suitable material and compacted per Section 4.3 of this report.
- Cobbles and boulders should be removed at least 6 inches from beneath footings and 18 inches beneath the bottom of slabs and paved areas. The resulting excavations should be backfilled with compacted Structural Fill under the building and with Ordinary Fill under the subbase of paved areas.
- The bottom of the excavation resulting from the removal of the existing fill or natural soil should be compacted with a dynamic vibratory compactor imparting a minimum of 40 kips of force to the subgrade.
- The base of the footing excavations in granular soil should be compacted with a dynamic vibratory compactor weighing at least 200 pounds and imparting a minimum of 4 kips of force to the subgrade.
- After the surficial materials are removed to a depth of 18 inches within the proposed paved areas in accordance with the recommendations in Section 3.1, the exposed existing fill and buried subsoil deeper than 18 inches beneath the bottom of the proposed pavement should be improved by compacting the exposed surface with at least six (6) passes of a vibratory roller compactor imparting a dynamic effort of at least 40 kips. Where soft zones of soil are observed, the soft soil should be removed, and the grade should be restored using Ordinary Fill to the bottom of the proposed subbase layer. If pumping of the existing fill or buried subsoil deeper than 18 inches beneath the bottom of the proposed pavement is observed, the soft and/or pumping material should be removed and replaced.
- Fill placed within the footprint of the proposed building should meet the gradation and compaction requirements of Structural Fill, shown in Section 4.3.1.
- Fill placed under the subbase of paved areas should meet the gradation and compaction requirements of Ordinary Fill, shown in Section 4.3.2.
- Fill placed in the top 12 inches beneath sidewalks should consist of Structural Fill with less than 5 percent fines.



- Loose or soft soils identified during the compaction of the footing or floor slab subgrades should be excavated to a suitable bearing stratum, as determined by the representative of LGCI. Grades should be restored by backfilling with Structural Fill or crushed stone.
- When crushed stone is required in the drawings or is used for the convenience of the contractor, it should be wrapped in a geotextile fabric for separation except where introduction of the geotextile fabric promotes sliding. A geotextile fabric should not be placed between the bottoms of the footings and the crushed stone.
- An LGCI representative should observe the exposed subgrades prior to fill and concrete placement to verify that the exposed bearing materials are suitable for the design soil bearing pressure. If soft or loose pockets are encountered in the footing excavations, the soft or loose materials should be removed and the bottom of the footing should be placed at a lower elevation on firm soil, or the resulting excavation should be backfilled with Structural Fill, or crushed stone wrapped in a filter fabric.
- APs that are damaged as a result of excavation for footings should be repaired in accordance with the requirements of the specialty contractor installing the APs.
- Before fill is placed under footings or to raise the grades, the aggregate piers should be exposed, and the subgrade should be compacted to a firm and unyielding conditions.
- An LGCI geotechnical representative should observe the installation of the aggregate piers and the modulus test. An LGCI geotechnical representative should also observe the exposed subgrades prior to fill and concrete placement to verify that the exposed the aggregate piers are properly exposed.

4.2 Subgrade Protection

The onsite fill and natural soils are frost susceptible. If construction takes place during freezing weather, special measures should be taken to prevent the subgrade from freezing. Such measures should include the use of heat blankets or excavating the final six inches of soil just before pouring the concrete. Footings should be backfilled as soon as possible after footing construction. Soil used as backfill should be free of frozen material, as should the ground on which it is placed. Filling operations should be halted during freezing weather.

Materials with high fines contents are typically difficult to handle when wet, as they are sensitive to moisture content variations. Subgrade support capacities may deteriorate when such soils become wet and/or disturbed. The contractor should keep exposed subgrades properly drained and free of ponded water. Subgrades should be protected from machine and foot traffic to reduce disturbance.



4.3 Fill Materials

Structural Fill and Ordinary Fill should consist of inert, hard, durable sand and gravel free from organic matter, clay, surface coatings, and deleterious materials, and should conform to the gradation requirements shown below.

4.3.1 Structural Fill

The Structural Fill should have a plasticity index of less than 6 and should meet the gradation requirements shown below. Structural Fill should be compacted in maximum 9-inch loose lifts to at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557), with moisture contents within ± 2 percentage points of the optimum moisture content.

Sieve Size Percent	Passing by Weight
3 inches	100
$1\frac{1}{2}$ inch	80-100
$\frac{1}{2}$ inch	50-100
No. 4	30-85
No. 20	15-60
No. 60	5-35
No. 200*	0-10

* 0-5 for the top 12 inches under sidewalks, exterior slabs, pads, and walkways

4.3.2 Ordinary Fill

Ordinary Fill should have a plasticity index of less than 6 and should meet the gradation requirements shown below. Ordinary Fill should be compacted in maximum 9-inch loose lifts to at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557), with moisture contents within ± 2 percentage points of the optimum moisture content.

Sieve Size Percent	Passing by Weight
6 inches	100
1 inch	50-100
No. 4	20-100
No. 20	10-70
No. 60	5-45
No. 200	0-20

4.4 Reuse of Onsite Materials

The reuse of the existing fill and excavated natural sand and gravel, if applicable, should be in accordance with the recommendations in Section 3.1.1. The buried topsoil and buried subsoil should be segregated from the existing fill before reusing and/or improving the existing fill.



The contractor should avoid mixing the reusable soils with fine-grained and/or organic soils. The soils to be reused should be excavated and stockpiled separately for compliance testing. Soils with 20 percent or greater fines contents are generally very sensitive to moisture content variations and are susceptible to frost. Such soils are very difficult to compact at moisture contents that are much higher or much lower than the optimum moisture content determined from the laboratory compaction test. Therefore, strict moisture control should be implemented during the compaction of onsite soils with fines contents of 20 percent or greater. The contractor should be prepared to remove and replace such soils if pumping occurs.

To improve the existing fill, the existing fill should be blended with ³/₄-inch or 1 ¹/₂-inch crushed stone at the ratio listed in Section 3.1.1. Grain-size analyses should be performed on the blended material and the blending ratio should be adjusted as needed based on the results of the grainsize analyses.

Due to the large scale of earth moving operations, we recommend that excavated materials slated for reuse be protected from wetness, including by means of tarps.

Materials to be used as fill should first be tested for compliance with the applicable gradation specifications.

4.5 Groundwater Control Procedures

Based on the groundwater levels measured in our borings, we do not anticipate that major groundwater control procedures will be needed during construction. We anticipate that filtered sump pumps installed in a series of sump pump pits located at least three feet below the bottom of planned excavations may be sufficient to handle groundwater and surface runoff that may enter the excavation during wet weather. The contractor should be prepared to use multiple sump pumps to maintain a dry excavation during the removal of the existing fill.

The contractor should be permitted to employ whatever commonly accepted means and practices are necessary to maintain the groundwater level below the bottom of the excavation and to maintain a dry excavation during wet weather. Groundwater levels should be maintained at a minimum of 1 foot below the bottom of the excavations during construction. The placement of reinforcing steel or concrete in standing water should not be permitted.

To reduce the potential for sinkholes developing over sump pump pits after the sump pumps are removed, the crushed stone placed in the sump pump pits should be wrapped in a geotextile fabric. Alternatively, the crushed stone should be entirely removed after the sump pump is no longer in use, and the sump pump pit should be restored with suitable backfill.

4.6 Temporary Excavations

All excavations to receive human traffic should be constructed in accordance with OSHA guidelines.



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The site soils should generally be considered Type "C" and should have a maximum allowable slope of 1.5 Horizontal to 1 Vertical (1.5H:1V) for excavations less than 20 feet deep. Deeper excavations, if needed, should have shoring designed by a professional engineer.

The contractor is solely responsible for designing and constructing stable, temporary excavations and should shore, slope, or bench the sides of the excavations as required to maintain the stability of the excavation sides and bottom.



5. RECOMMENDATIONS FOR FUTURE WORK

We recommend engaging LGCI to perform the following services:

- Prepare Earth Moving Specifications and APs, if needed, and review the geotechnical aspect of contract drawings.
- Review contractor submittals and Request for Information (RFIs);
- Provide a field engineer during construction to observe the removal of the unsuitable soil, the improvement of the existing fill, to observe the subgrade of footings and slabs, and to observe the installation of ground improvement as well as the modulus test, if the ground improvement option is selected.



6. REPORT LIMITATIONS

Our analyses and recommendations are based on project information provided to us at the time of this report. If changes to the type, size, and location of the proposed structures or to the site grading are made, the recommendations contained in this report shall not be considered valid unless the changes are reviewed, and the conclusions and recommendations modified in writing by LGCI. LGCI cannot accept responsibility for designs based on our recommendations unless we are engaged to review the final plans and specifications to determine whether any changes in the project affect the validity of our recommendations, and whether our recommendations have been properly implemented in the design.

It is not part of our scope to perform a more detailed site history; therefore, we have not explored for or researched the locations of buried utilities or other structures in the area of the proposed construction. Our scope did not include environmental services or services related to moisture, mold, or other biological contaminants in or around the site.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from anticipated conditions are encountered, it may be necessary to revise the recommendations in this report. We cannot accept responsibility for designs based on recommendations in this report unless we are engaged to 1) make site visits during construction to check that the subsurface conditions exposed during construction are in general conformance with our design assumptions and 2) ascertain that, in general, the work is being performed in compliance with the contract documents.

Our report has been prepared in accordance with generally accepted engineering practices and in accordance with the terms and conditions set forth in our agreement. No other warranty, expressed or implied, is made. This report has been prepared for the exclusive use of Taco Comfort Solutions for the Proposed Manufacturing Building in Cranston, Rhode Island as conceived at this time.



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7. REFERENCES

In addition to the references included in the text of the report, we used the following references:

Rhode Island State Building Code (Feb. 2022), comprised of the International Building Code of 2018 (IBC-2018) and RI amendments.

The Department of Labor, Occupational Safety and Health Administration (1989), "Occupational Safety and Health Standards - Excavations; Final Rule," 20 CFR Part 1926, Subpart P.

USGS Cranston, RI topographic map from http://mapserver.mytopo.com.



Table 1 -Summary of LGCI's Test Pits
Proposed Manufacturing Building
Cranston, RI
LGCI Project No. 2252

Test Pit No.	Ground Surface Elevation (ft.) ¹	Groundwater ² Depth / El. (ft.)	Bottom of Asphalt / Topsoil Depth / El. (ft.)	Bottom of Crushed Stone Depth / El. (ft.)	Bottom of Fill Depth / El. (ft.)	Bottom of Buried Organic Soil / Buried Subsoil Depth / El. (ft.)	Bottom of Sand and Gravel Depth / El. (ft.)	Bottom of Test Pit Depth / El. (ft.)
TP-1	56.0	10.0 / 46.0	0.3 / 55.7	- / -	4.0 / 52.0	5.0 / 51.0	10.0 ³ / 46.0	10.0 / 46.0
TP-2	55.0	9.5 / 45.5	0.3 / 54.7	- / -	5.5 / 49.5	- / -	10.0 ³ / 45.0	10.0 / 45.0
TP-3	57.0	10.0 / 47.0	0.3 / 56.7	- / -	4.0 / 53.0	5.0 / 52.0	10.3 ³ / 46.7	10.3 / 46.7
TP-4	56.0	10.5 / 45.5	0.3 / 55.7	- / -	6.5 / 49.5	9.0 / 47.0	11.0 ³ / 45.0	11.0 / 45.0
TP-5	56.0	12.0 / 44.0	2.0 / 54.0	- / -	6.7 / 49.3	7.7 / 48.3	12.0 ³ / 44.0	12.0 / 44.0
TP-6	59.0	- / -	1.5 / 57.5	- / -	8.5 / 50.5	11.0 / 48.0	12.0 ³ / 47.0	12.0 / 47.0
TP-7	62.0	- / -	2.0 / 60.0	- / -	- / -	- / -	10.0 ³ / 52.0	10.0 / 52.0
TP-8	64.0	- / -	- / -	0.3 / 63.7	5.5 / 58.5	- / -	9.0 ³ / 55.0	9.0 / 55.0
TP-9	67.0	- / -	- / -	0.3 / 66.7	5.0 / 62.0	- / -	10.0 ³ / 57.0	10.0 / 57.0
TP-10	62.0	- / -	0.8 / 61.2	- / -	6.5 / 55.5	- / -	10.0 ³ / 52.0	10.0 / 52.0
TP-11	68.0	- / -	0.3 / 67.7	- / -	1.5 / 66.5	- / -	9.0 ³ / 59.0	9.0 / 59.0
TP-12	69.0	- / -	0.5 / 68.5	- / -	1.0 / 68.0	- / -	10.0 ³ / 59.0	10.0 / 59.0
TP-13	68.0	- / -	0.3 / 67.7	- / -	5.0 / 63.0	- / -	10.0 ³ / 58.0	10.0 / 58.0
TP-14	65.0	- / -	- / -	0.3 / 64.7	6.0 / 59.0	- / -	9.0 ³ / 56.0	9.0 / 56.0
TP-15	63.0	- / -	- / -	0.3 / 62.7	4.0 / 59.0	- / -	9.0 ³ / 54.0	9.0 / 54.0

1. The ground surface elevation was interpolated to the nearest foot from drawing C-200 titled: "Civil Proposed Site Plan," prepared by Woodard & Curran, dated August 2022, and provided to LGCI by Thermo-Mechanical Systems Corporation via e-mail on August 23, 2022.

2. Groundwater was measured during excavation, at the end of excavation, after excavation, or based on sample moisture whichever is shallower.

3. Test pit terminated in the sand and gravel layer.

4. "-" means groundwater or layer was not encountered.

Table 2 - Summary of LGCI's Borings Proposed Manufacturing Building Cranston, RI LGCI Project No. 2252

Boring No.	Ground Surface Elevation (ft.) ¹	Groundwater ² Depth / El. (ft.)	Bottom of Asphalt / Topsoil / <i>Crushed Stone</i> Depth / El. (ft.)	Bottom of Fill Depth / El. (ft.)	Bottom of Buried Organic Soil Depth / El. (ft.)	Bottom of Sand and Gravel Depth / El. (ft.)	Bottom of Silt Depth / El. (ft.)	Top of Rock / Weathered Rock Depth / El. (ft.)	Bottom of Boring Depth / El. (ft.)
				20	22 Borings				
B-1	58.0	- / -	0.3 / 57.7	8.0 / 50.0	- / -	12.0 ³ / 46.0	- / -	- / -	12.0 / 46.0
B-2	57.0	8.0 / 49.0	0.3 / 56.7	8.0 / 49.0	10.0 / 47.0	12.0 ³ / 45.0	- / -	- / -	12.0 / 45.0
B-3	58.0	12.0 / 46.0	0.3 / 57.7	6.0 / 52.0	- / -	22.0 ³ / 36.0	- / -	- / -	22.0 / 36.0
B-4	58.0	10.0 / 48.0	0.3 / 57.7	6.0 / 52.0	8.0 / 50.0	22.0 ³ / 36.0	- / -	- / -	22.0 / 36.0
B-5	60.0	14.0 / 46.0	0.2 / 59.8	8.0 / 52.0	- / -	22.0 ³ / 38.0	- / -	- / -	22.0 / 38.0
B-6	60.0	10.0 / 50.0	0.3 / 59.7	8.0 / 52.0	- / -	22.0 ³ / 38.0	- / -	- / -	22.0 / 38.0
B-7	61.0	14.0 / 47.0	0.7 / 60.3	10.0 / 51.0	- / -	22.0 ³ / 39.0	- / -	- / -	22.0 / 39.0
B-8	63.0	19.0 / 44.0	0.3 / 62.7	8.0 / 55.0	- / -	22.0 ³ / 41.0	- / -	- / -	22.0 / 41.0
B-9	65.0	19.0 / 46.0	0.3 / 64.7	6.0 / 59.0	- / -	22.0 ³ / 43.0	- / -	- / -	22.0 / 43.0
B-10	66.0	19.0 / 47.0	0.3 / 65.7	6.0 / 60.0	- / -	21.0 ³ / 45.0	- / -	- / -	21.0 / 45.0
B-11	68.0	- / -	0.5 / 67.5	6.5 / 61.5	- / -	22.0 ³ / 46.0	- / -	- / -	22.0 / 46.0
B-12	66.0	20.0 / 46.0	0.3 / 65.7	2.0 / 64.0	- / -	22.0 ³ / 44.0	- / -	- / -	22.0 / 44.0
B-13	67.0	20.0 / 47.0	0.2 / 66.8	4.0 / 63.0	- / -	22.0 ³ / 45.0	- / -	- / -	22.0 / 45.0
B-14	68.0	22.0 / 46.0	0.3 / 67.7	4.0 / 64.0	- / -	22.0 ³ / 46.0	- / -	- / -	22.0 / 46.0
B-15	59.0	13.0 / 46.0	0.3 / 58.7	10.4 / 48.6	- / -	22.0 ³ / 37.0	- / -	- / -	22.0 / 37.0
B-16	56.0	10.0 / 46.0	0.4 / 55.6	6.8 / 49.2	- / -	12.0 ³ / 44.0	12.0 ³ / 44.0	- / -	12.0 / 44.0
B-17	61.0	20.0 / 41.0	0.3 / 60.7	4.0 / 57.0	- / -	22.0 ³ / 39.0	- / -	- / -	22.0 / 39.0
				20	23 Borings				
B-101	58.0	8.0 / 50.0	0.3 / 57.7	10.5 / 47.5	- / -	33.0 / 25.0	45.0 / 13.0	45.0 ⁴ / 13.0	53.5 / 4.5
B-102	57.0	6.0 / 51.0	0.3 / 56.7	12.0 / 45.0	10.0 / 47.0	44.0 / 13.0	39.0 / 18.0	44.0 ⁴ / 13.0	49.0 / 8.0

1. The ground surface elevation was interpolated to the nearest foot from drawing C-200 titled: "Civil Proposed Site Plan," prepared by Woodard &

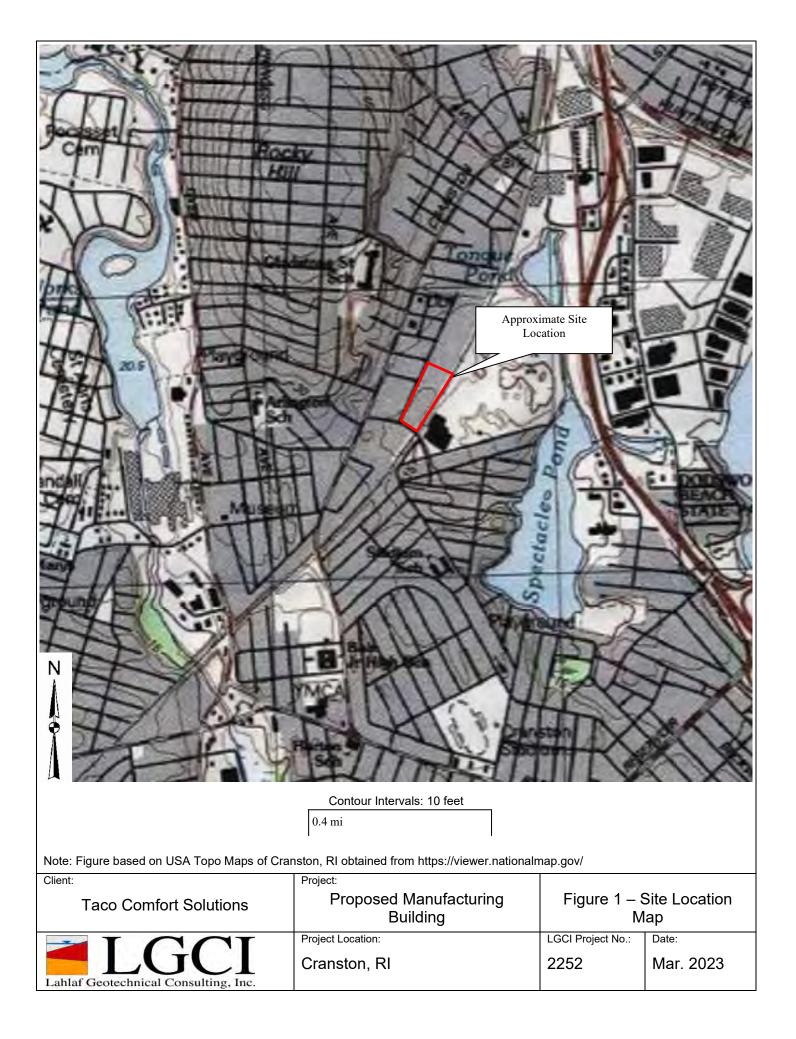
Curran, dated August 2022, and provided to LGCI by Thermo-Mechanical Systems Corporation via e-mail on August 23, 2022.

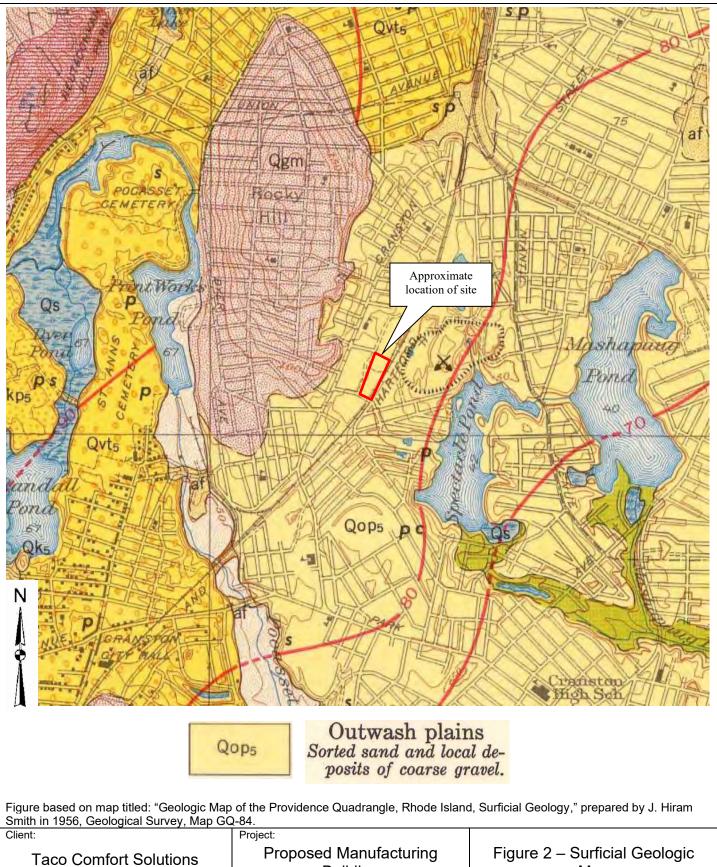
2. Groundwater was measured during drilling, at the end of drilling, after drilling, or based on sample moisture whichever is shallower.

3. Boring terminated in the sand and gravel layer.

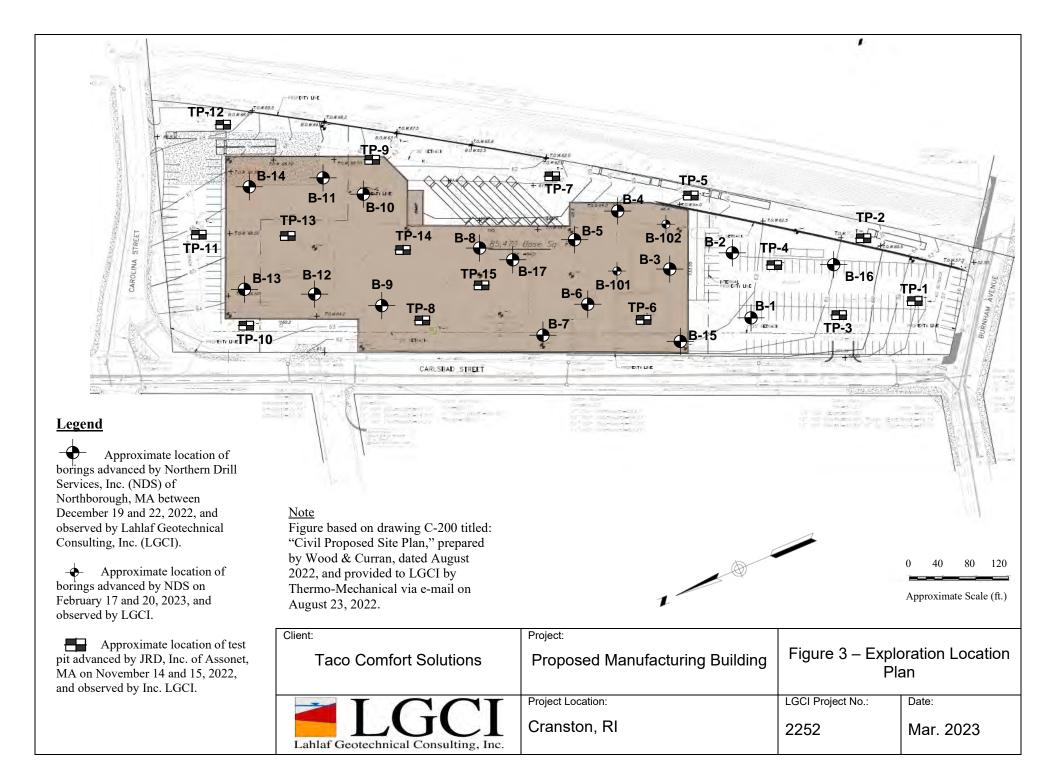
4. Boring terminated in rock.

5. "-" means groundwater or layer was not encountered.

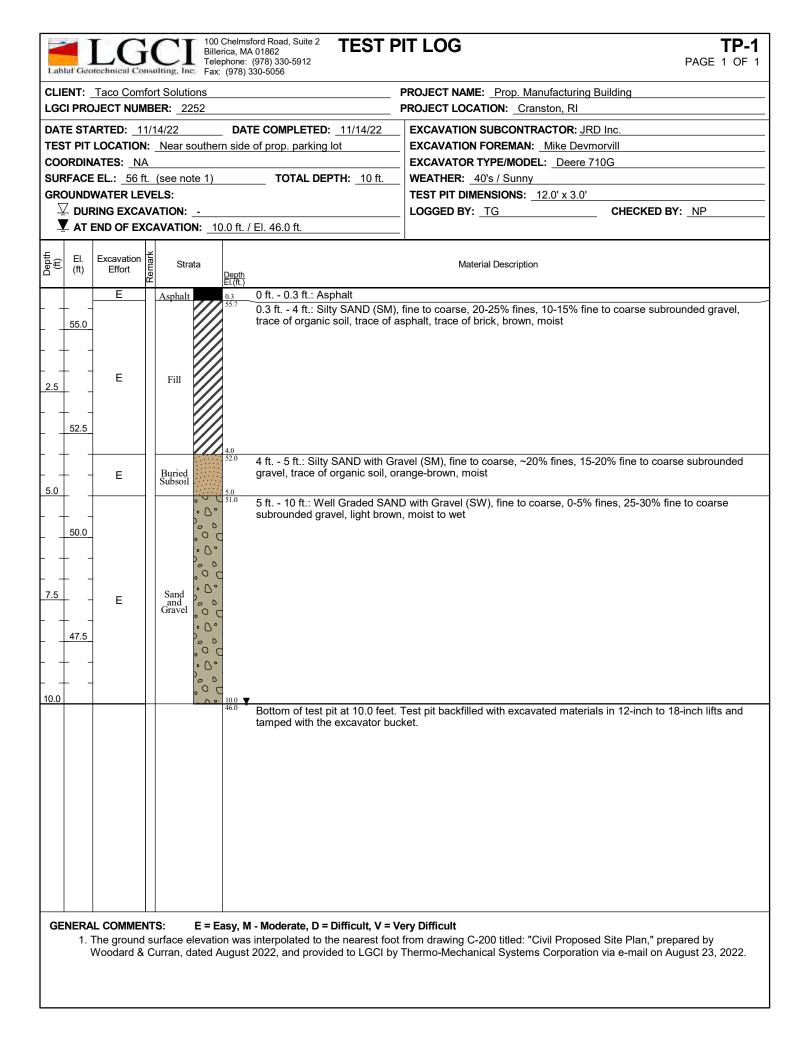


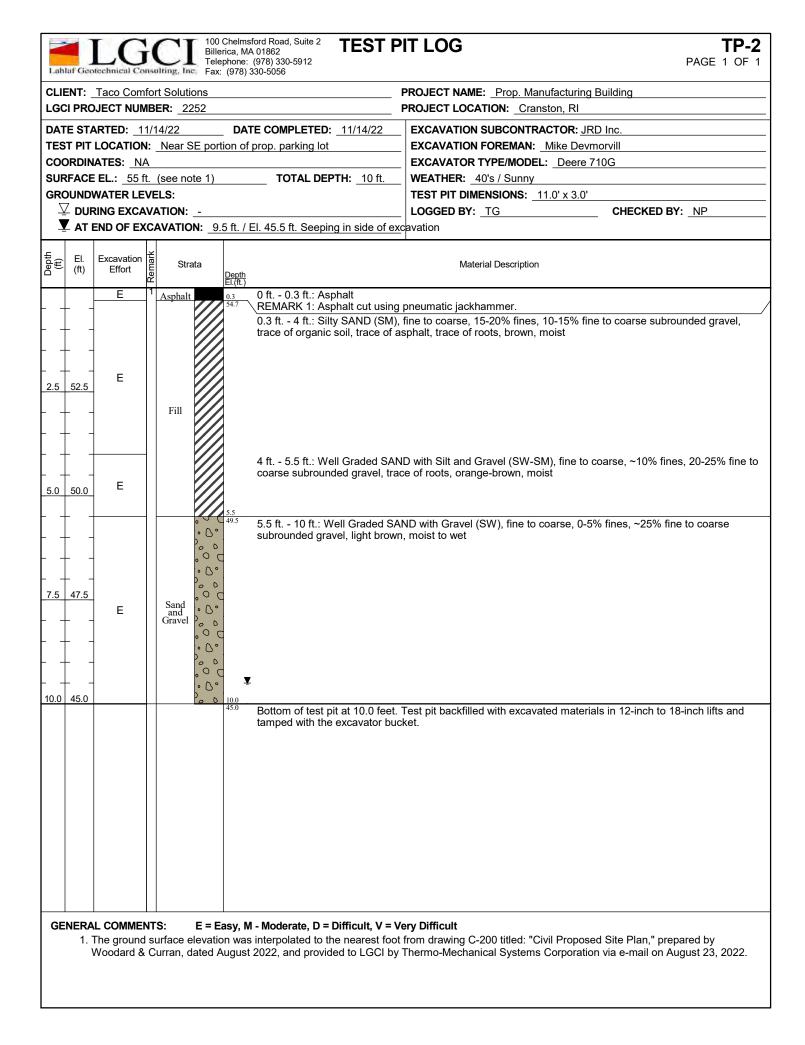


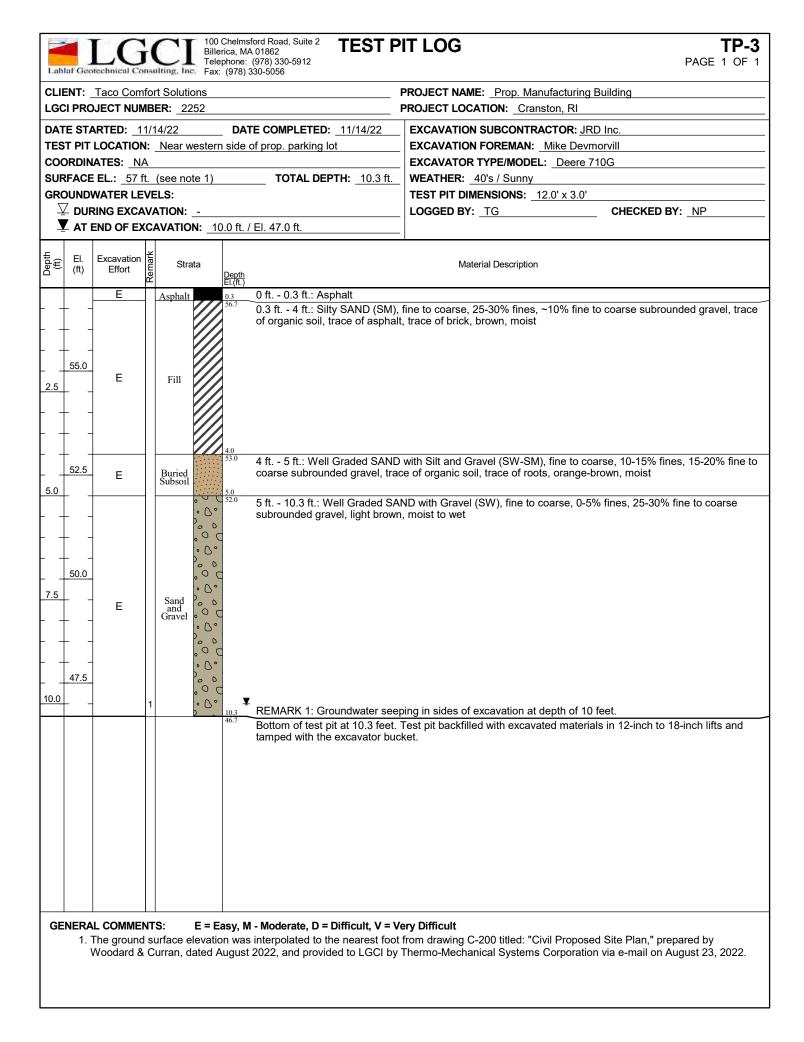
Taco Comfort Solutions	Building	Figure 2 – Surficial Geologic Map	
Lahlaf Geotechnical Consulting, Inc.	Project Location:	LGCI Project No.:	^{Date:}
	Cranston, RI	2252	Mar. 2023

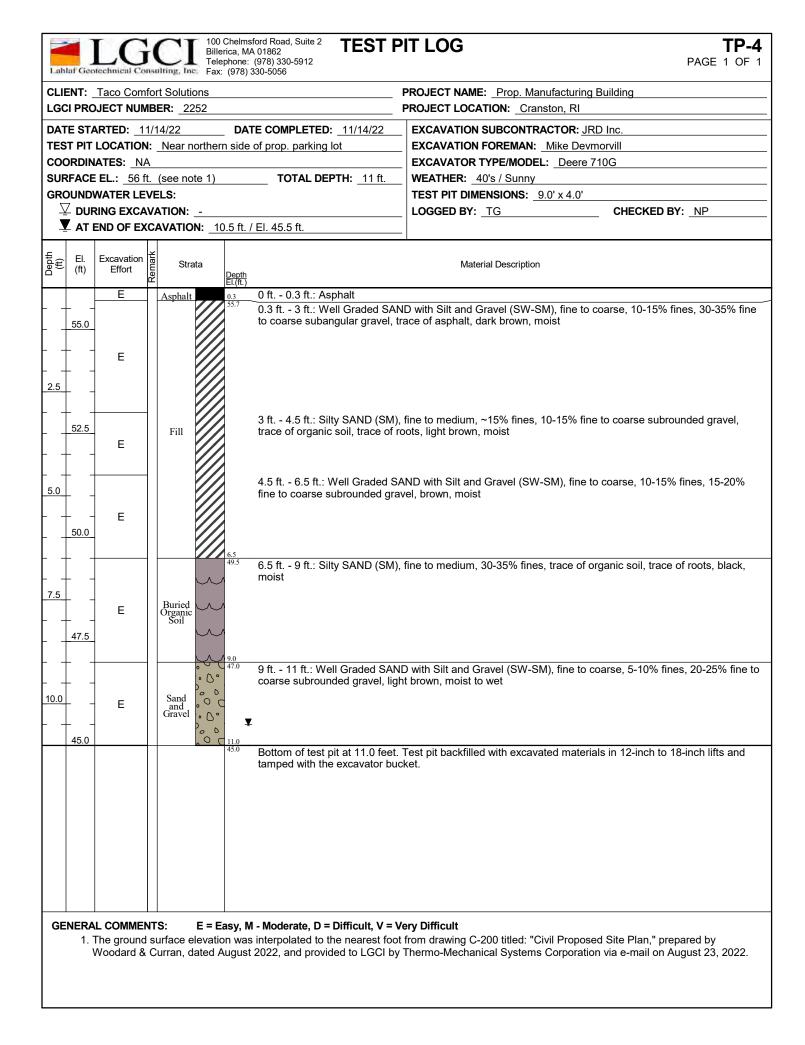


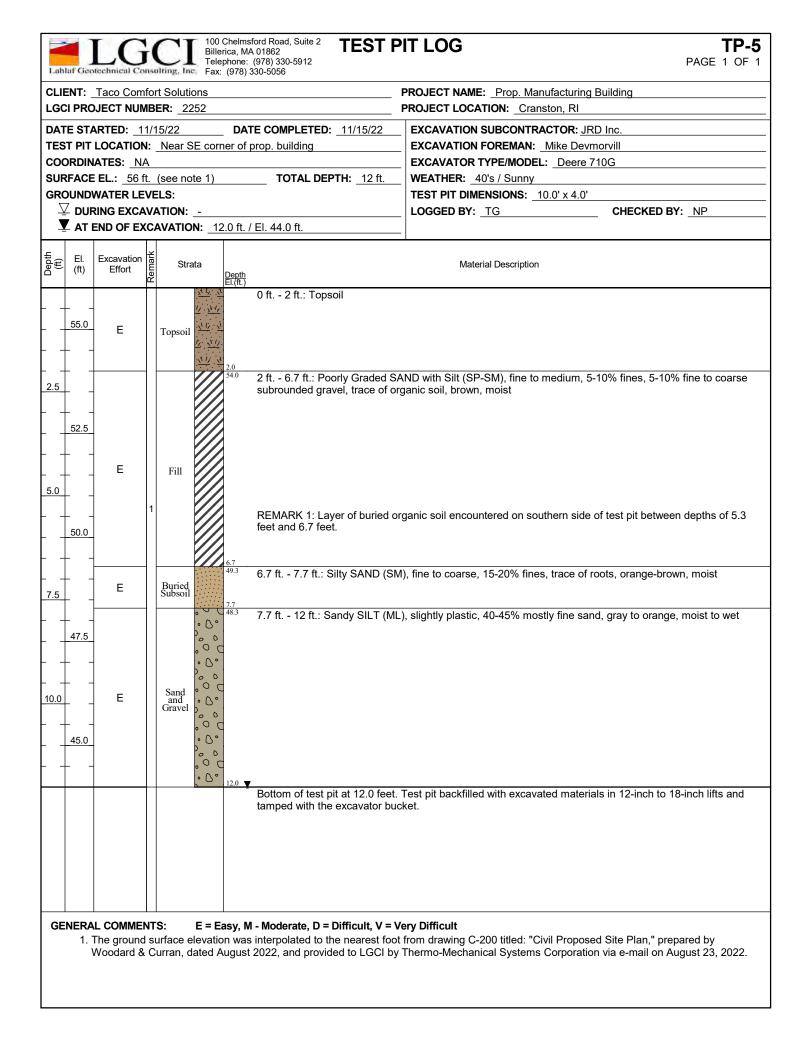
Appendix A – LGCI's Test Pit Logs

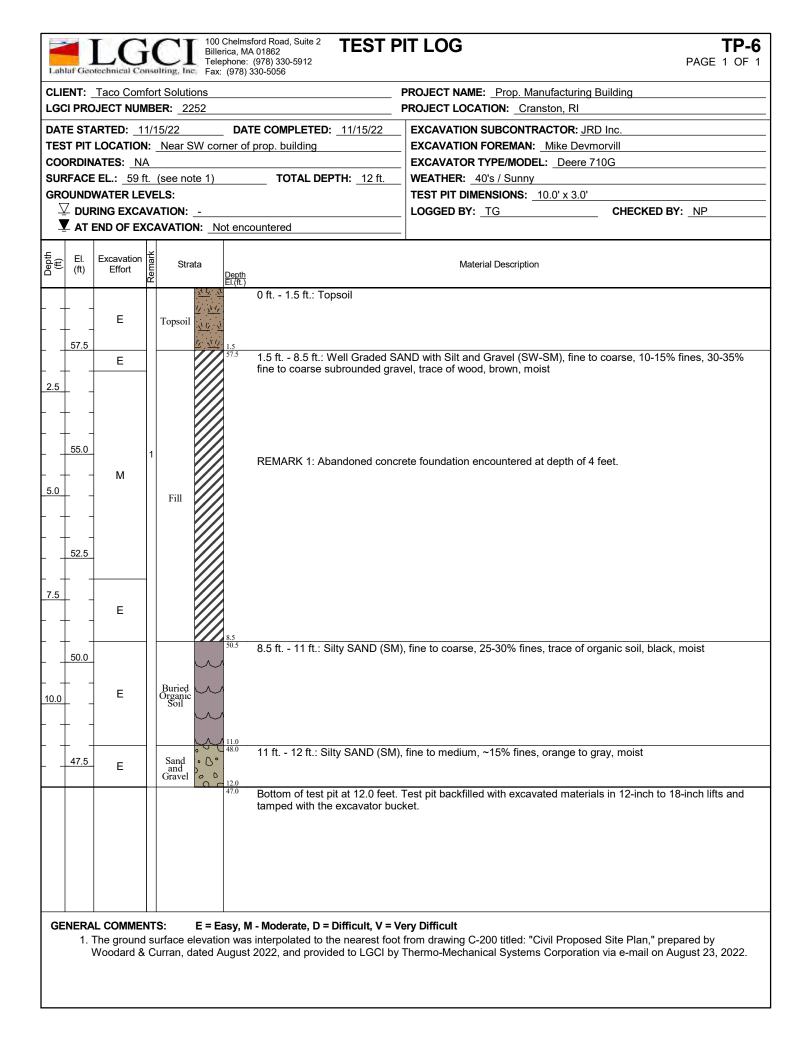




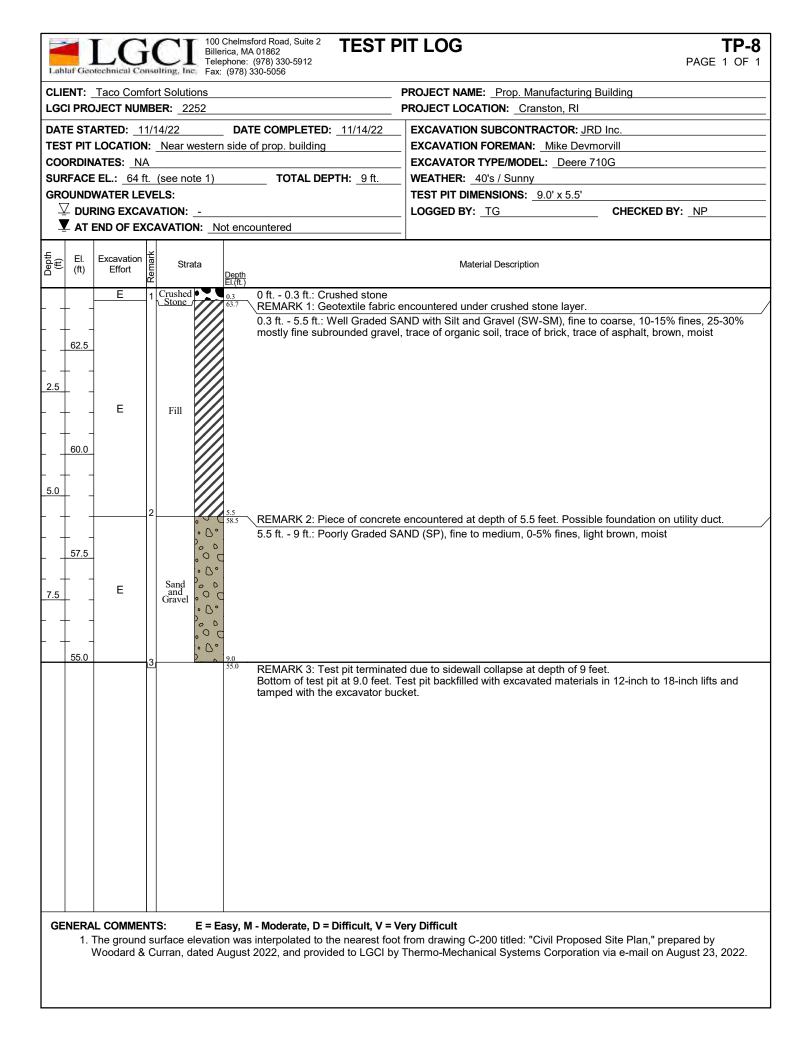


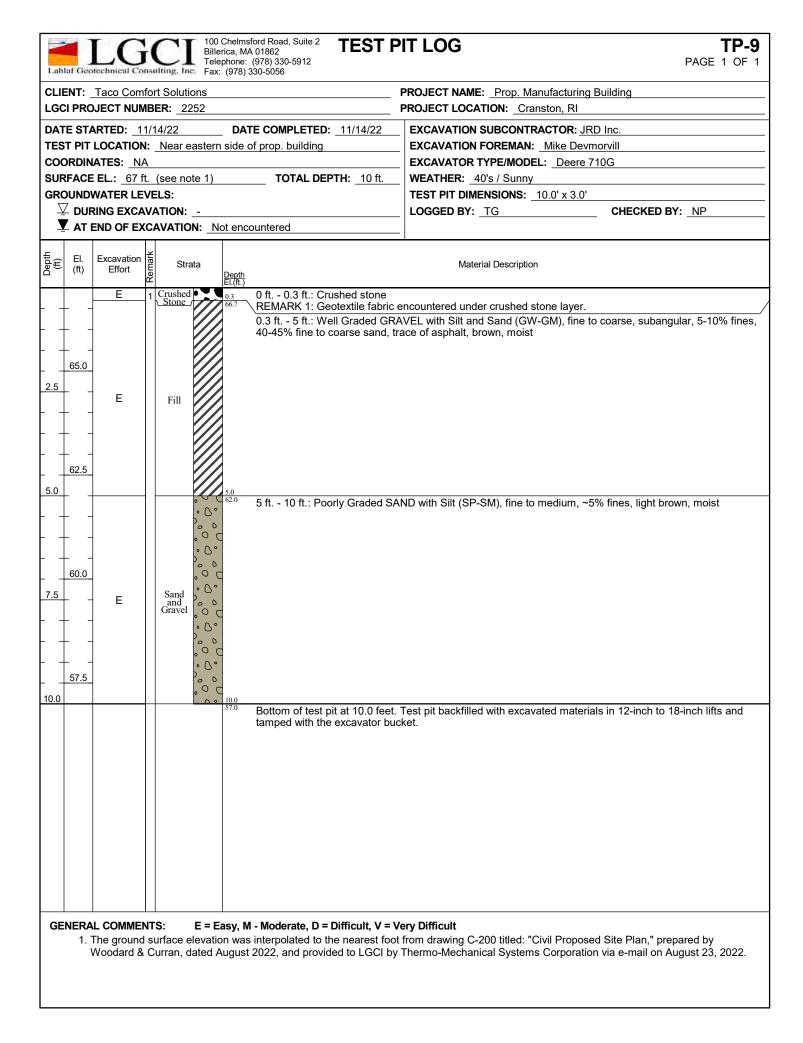


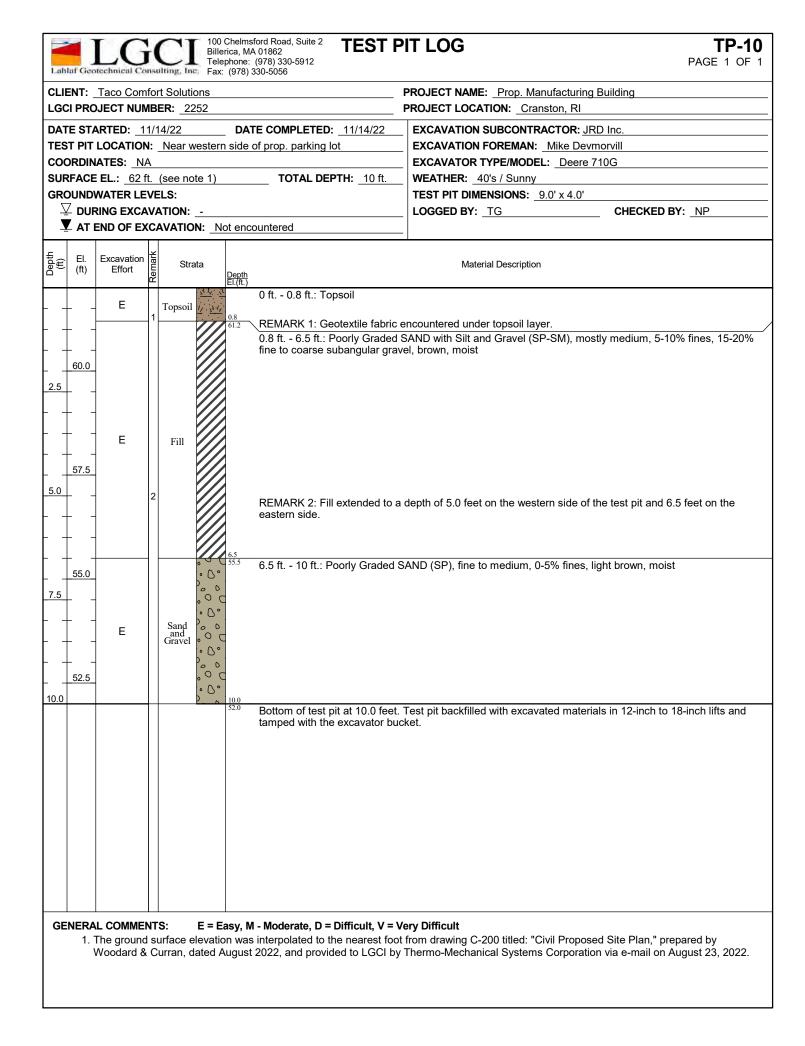


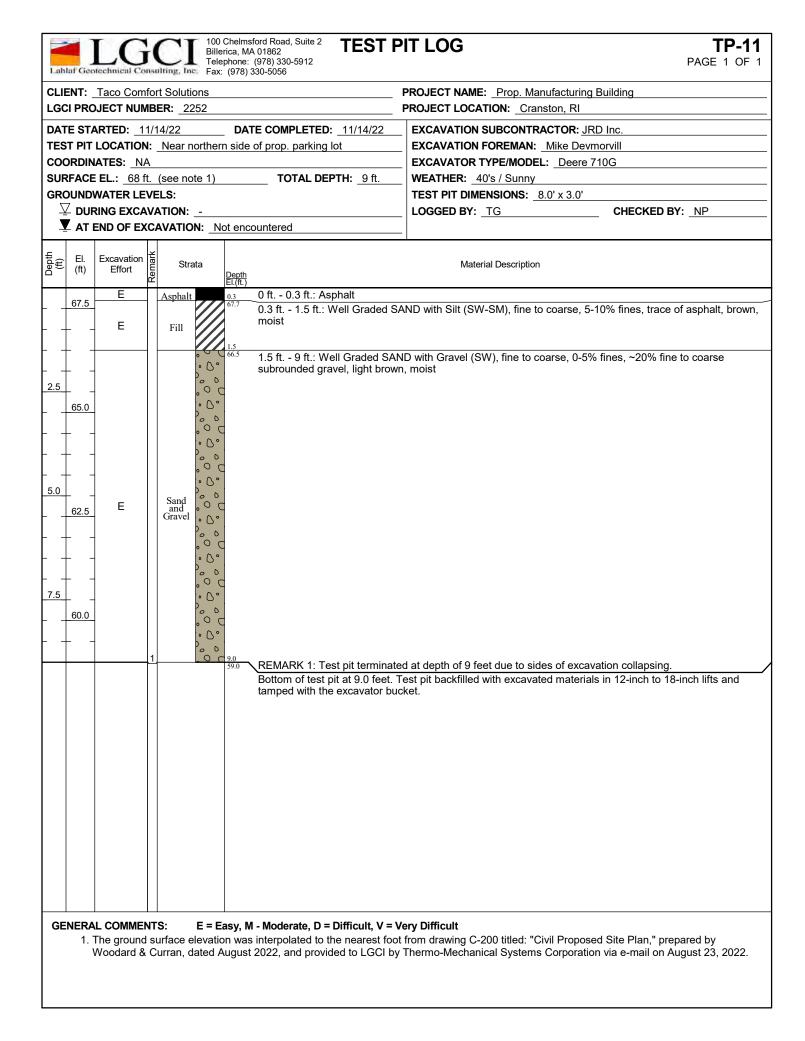


	Taco Con JECT NU				PROJECT NAME: Prop. Manufacturing Building				
					PROJECT LOCATION: Cranston, I				
				ATE COMPLETED: <u>11/15/22</u> parking and loading dock	EXCAVATION SUBCONTRACTOR EXCAVATION FOREMAN: Mike				
	ATES: N		prop. trailer						
			note 1)	TOTAL DEPTH: 10 ft.	WEATHER: 40's / Sunny				
					TEST PIT DIMENSIONS: 8.0' × 3	:.0'			
	RING EXC		l: -		LOGGED BY: TG				
			ION: Not er	ncountered	_				
EI.	Excavation	ž							
E El. (ft)	Effort	Remark S	itrata Depi El.(fi	<u>h</u>	Material Description				
			EI.(fl	.) 0 ft 2 ft.: Topsoil					
+ +			<u>1/ x11/</u>	•••• =•••••					
+ -	Е	Topso							
		Topse							
60.0			<u>1/</u> 2.0						
		1	o		AND with Gravel (SP), mostly medium	, 0-5% fines, 25-30% fine to coarse			
<u>i</u> -			° 0 °	angular gravel, brown, moist					
+ -			• C						
	М		° ° °						
57.5			• 0 °						
			000						
)			• O • C	5 ft - 10 ft · Poorly Graded S	SAND with Silt (SP-SM), fine to mediur	m 5-10% fines light brown moist			
+ -			200	on To h. Toony Graded c		in, 3-10% intes, light brown, moist			
		Sanç	1 ° C						
T		Sand and Grave							
+			°°C						
55.0			° 0 °						
54 -	Е								
			° 0 °						
			00						
— –			° 0 °						
+ +			200						
52.5			° 0 C						
0			• \ ° _{10.0}						
			52.0	Bottom of test pit at 10.0 fee tamped with the excavator b	t. Test pit backfilled with excavated m	aterials in 12-inch to 18-inch lifts and			
			I						
	L COMME			M - Moderate, D = Difficult, V =	N/ D'// H				

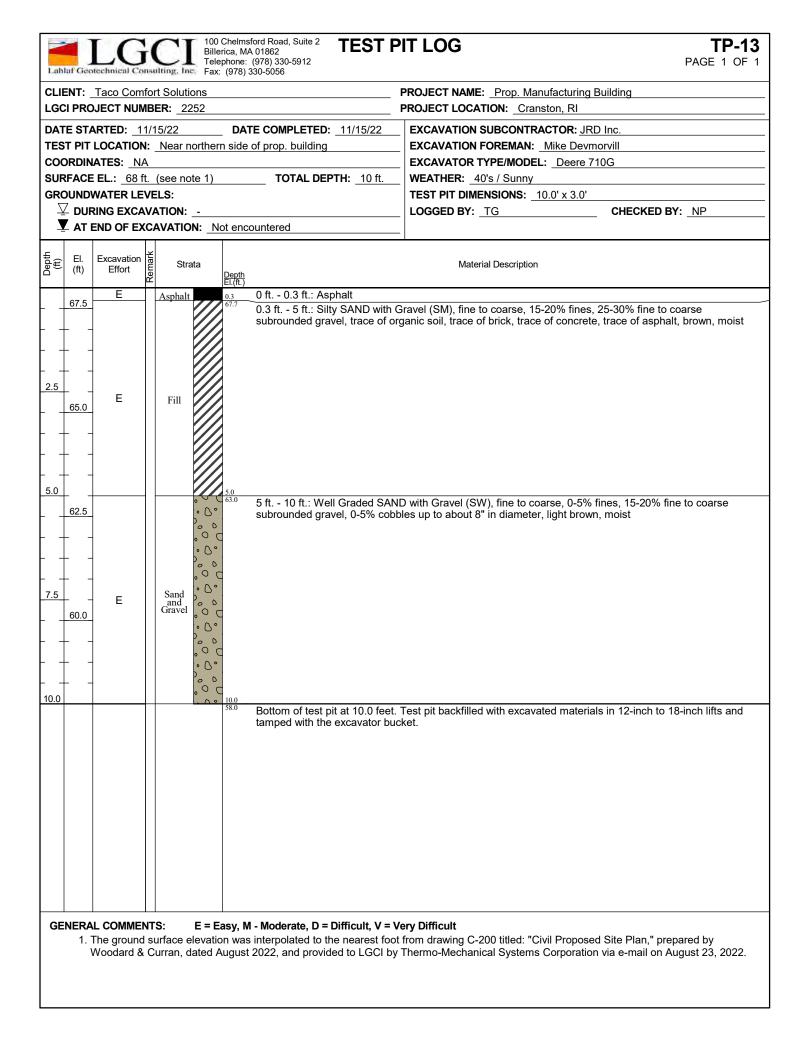


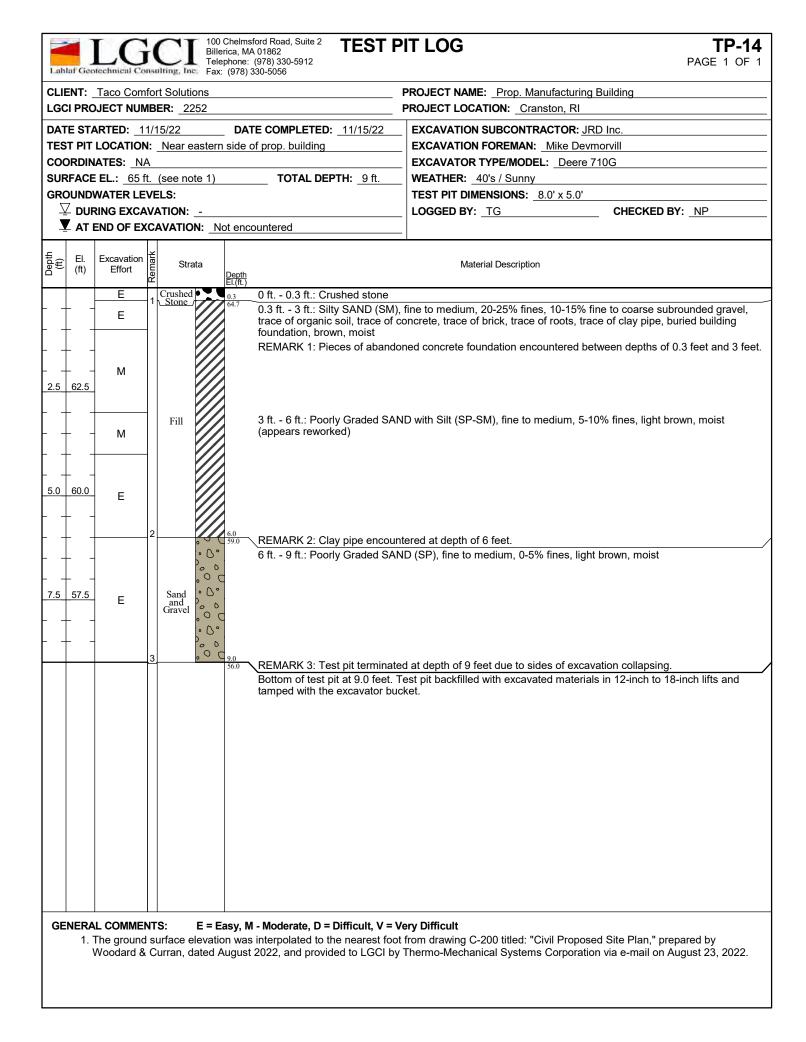


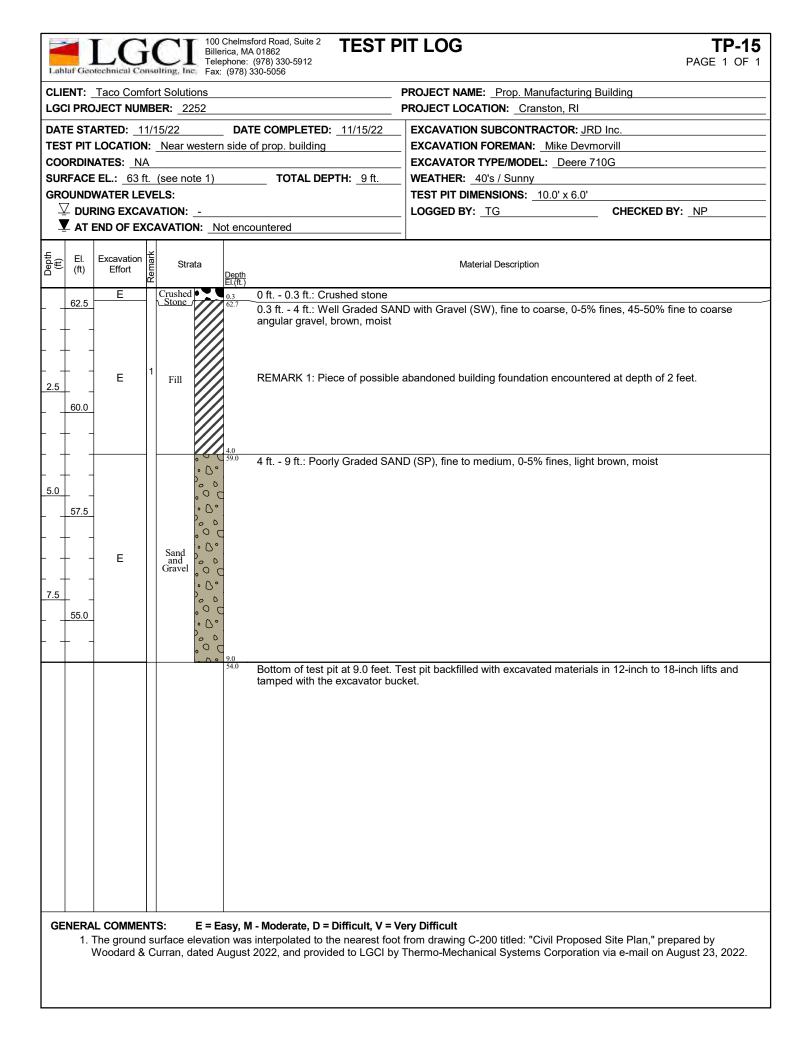




ahlaf Geotechnical Consulting, Inc. Fax: (978) 330-5056	PROJECT NAME: Prop. Manufacturing Building				
GCI PROJECT NUMBER: _2252	PROJECT LOCATION: Cranston, RI				
ATE STARTED: 11/14/22 DATE COMPLETED: 11/14/22	EXCAVATION SUBCONTRACTOR: JRD Inc.				
EST PIT LOCATION: Near NE corner of prop. parking lot	EXCAVATION FOREMAN: Mike Devmorvill				
OORDINATES: NA	EXCAVATOR TYPE/MODEL: Deere 710G				
URFACE EL.: <u>69 ft.</u> (see note 1) TOTAL DEPTH: <u>10 ft.</u> ROUNDWATER LEVELS:	WEATHER: _40's / Sunny TEST PIT DIMENSIONS: _8.0' x 5.0'				
\overline{Y} DURING EXCAVATION: -	LOGGED BY: TG CHECKED BY: NP				
T AT END OF EXCAVATION: Not encountered					
$\begin{array}{c c} \widehat{El.} & Excavation & \overleftarrow{tr} \\ (ft) & Effort & \overleftarrow{tr} \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ \hline \end{array} \right) Strata \\ & & & \\$	Material Description				
E 1 Topsoil 0 ft 0.5 ft.: Topsoil					
68.5 REMARK 1: Geotextile fabric	c encountered under topsoil layer. ND with Silt and Gravel (SW-SM), fine to coarse, 5-10% fines, 25-30% fine				
to coarse subrounded gravel	, trace of organic soil, light brown, moist				
	ND with Silt and Gravel (SW-SM), fine to coarse, 5-10% fines, 25-30% fine -10% cobbles up to about 6 inches in diameter, light brown, moist				
65.0					
Sand Sol					
<u>• • C</u>					
60.0 ° °					
1.0 10.0					
^{59.0} Bottom of test pit at 10.0 fee tamped with the excavator b	t. Test pit backfilled with excavated materials in 12-inch to 18-inch lifts and				
GENERAL COMMENTS: E = Easy, M - Moderate, D = Difficult, V =					
1. The ground surface elevation was interpolated to the nearest for	ot from drawing C-200 titled: "Civil Proposed Site Plan." prepared by				







Appendix B – LGCI's Boring Logs

Lahlaf G	Jeotec	chnic		Billeri	helmsford Rc ca, MA 01862 hone: 97833 9783305056	2	BO	RING	BLOG B-1 PAGE 1 OF 1		
CLIENT	: <u> </u>	aco	Comfort	t Solutions				PF	ROJECT NAME: Prop. Manufacturing Building		
LGCI PI	ROJI	ЕСТ	NUMBE	R : 2252				PF	PROJECT LOCATION: Cranston, RI		
				2/22			12/22/	22	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.		
				Near NW corne	er of prop.	parking lot					
COORD				see note 1)			тц. 47) #	DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig		
WEATH		_				IUTAL DEP		2 11.	HAMMER TYPE: Automatic		
GROUN									HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.		
ΣD	URIN	IG C	RILLIN	G: Not encou	ntered				SPLIT SPOON DIA.: 1.375 in. I.D., 2 in. O.D.		
				ING: Dry at t	he end of	drilling			CORE BARREL SIZE: NA		
⊻ o	THE	R: _	-						LOGGED BY: TG CHECKED BY: NP		
(ft.) (ft.) (ft.	.) Samble		Sample Number	Blow Counts (N Value)	Pen./Rec. te	Strata	Depth El.(ft.)		Material Description		
	0).5	Λ			Asphalt	0.3 57.7	_ Top 4'	": Asphalt silty SAND (SM), fine to coarse, 20-25% fines, 5-10% fine subrounded		
		2	S1	2-3-6 (9)	18/12			gravel	, trace of organic soil, trace of asphalt, brown, moist Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10%		
55.	.0	4	S2	6-7-3-2 (10)	24/13			fines,	15-20% fine to coarse subrounded gravel, brown, moist		
5	_		S3	4-5-2-2 (7)	24/9	Fill		soil, tr Bot. 6	op 3": Silty SAND (SM), fine to medium, 20-25% fines, trace of organic ace of asphalt, brown, moist ": Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5 fines, 15-20% fine to coarse subangular gravel, brown, moist		
		6	S4	3-3-2-2 (5)	24/15		8.0		ilty SAND (SM), fine to medium, 20-25% fines, trace of organic soil, dark , moist		
 10	_	8	S5	2-2-6-9 (8)	24/19	Sand and	2° 0	S5 - P light b	oorly Graded SAND with Silt (SP-SM), fine to medium, 10-15% fines, rown, moist		
	_	10	S6	16-29-24-25 (53)	24/15	。 <	0	S6 - V fines,	Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 30-35% fine to coarse angular gravel, light brown, moist		
45.		12						Bottor surfac	n of borehole at 12.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.		
15	_										
+	-										
+ +	-										
40.	.0										
20											
	1										
+	-										
+ $+$	-										
35.	.0										
25											
GENER	RAL	NOT	ES:	I	I	1	I				

Lahlaf Geo	otechni		Billeri	Chelmsford F ica, MA 018 phone: 9783 978330505	62 305912	2	BORIN	G LOG B-2 PAGE 1 OF 1
			Solutions					PROJECT NAME: Prop. Manufacturing Building
			R : <u>2252</u>					PROJECT LOCATION: Cranston, RI
			2/22					DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.
			lear NE corne	er of prop.	parking	lot		DRILLING FOREMAN: Tim Tucker
			see note 1)		TOTA		J. 10 ff	DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig
WEATHE					IUIA		1. <u>12 il.</u>	HAMMER TYPE: _Automatic
GROUND			-					HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.
			G: <u>8.0 ft. / El</u>	. 49.0 ft. E	Based o	n sample	e moisture	SPLIT SPOON DIA: 1.375 in. I.D., 2 in. O.D.
			ING: 9.0 ft. /					CORE BARREL SIZE: NA
То ⊈								LOGGED BY: TG CHECKED BY: NP
(ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Remark	Strata	<u>Depth</u> El.(ft.)	Material Description
	0.5-				Asph	alt _		3": Asphalt
	2-	S1	11-10-5 (15)	18/14			1	- Silty SAND with Gravel (SM), fine to coarse, 15-20% fines, 15-20% fine to rse subrounded gravel, trace of organic soil, brown, moist
- + -		S2	6-4-5-6 (9)	24/5			S2 fine	- Poorly Graded SAND with Silt and Gravel (SP-SM), fine to medium, 5-10% s, 25-30% coarse angular gravel, trace of concrete, light brown, moist
	4-	S3	6-4-2-2 (6)	24/7	Fill		S3	- Similar to S2, trace of organic soil
50.0	6-	S4	4-4-3-2 (7)	24/11			S4	- Similar to S2, trace of organic soil
- + - - + - 10	8-	S5	0-2-7-4 (9)	24/10	Burio Organ Soi	nic M	^{8.0} ^{49.0} S5 ▼ ang 10.0	- Silty SAND (SM), fine to medium, 25-30% fines, 5-10% fine to coarse ular gravel, trace of organic soil, black, wet
45.0	10-	S6	6-6-4-4 (10)	24/16	Sand a Grav	and ° °	- ^{47.0} S6	- Silty SAND (SM), fine, 20-25% fines, gray, wet
							Sur	tom of borehole at 12.0 feet. Borehole backfilled with drill cuttings. Ground ace restored with asphalt cold patch.
GENERA		TES:						
	-	-	alovation was	intorpolat	od to th	o pooros	t fact from	drawing C-200 titled: "Civil Proposed Site Plan " prepared by Woodard &

Lahlaf Geotechnical C		Chelmsford Rd rica, MA 01862 phone: 978330 9783305056		BLOG B-3 PAGE 1 OF 1
CLIENT: Taco Cor				ROJECT NAME: Prop. Manufacturing Building ROJECT LOCATION: Cranston, RI
DATE STARTED: BORING LOCATION COORDINATES: _M SURFACE EI.: _58 WEATHER: _30's / GROUNDWATER LI ☑ DURING DRILI ☑ DURING DRILI ☑ AT END OF D ☑ OTHER:	I2/21/22 I: _Near SE corne IA it. (see note 1) Sunny EVELS: LING: _15.0 ft. / f	EI. 43.0 ft. B	MPLETED: 12/21/22 uilding	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc. DRILLING FOREMAN: Tim Tucker DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb. HAMMER WEIGHT: 140 lb. You and the state of the st
Depth (ft.) Sample Interval (ft.)		Pen./Rec.	Strata Depth EI.(ft.)	Material Description
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S1 22-10-8 (18) S2 6-6-5-6 (11) S3 2-5-5-3 (10) S4 5-6-5-4 (11) S5 7-18-14-12 (32) S6 5-4-9-19 (13)	18/17 24/15 24/15 24/14 24/22 24/22 24/22	Asphalt 0.3 Top 4' S1 - W fine st Fill 57.7 S1 - W fine st S2 - S soil S3 - W fines, moist 6.0 S2.0 S4 - W S5.0 S5 - S Sand and S5 - S Sand and S7	 <u>* Asphalt</u> Vell Graded SAND with Silt (SW-SM), fine to coarse, 5-10% fines, 0-5% brounded gravel, light brown, moist imilar to S1, 10-15% fine to coarse subangular gravel, trace of organic Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% ~15% fine to coarse subrounded gravel, trace of organic soil, brown, Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% ~15% fine to coarse subrounded gravel, trace of organic soil, brown, Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% ~15% fine to coarse subrounded gravel, brown, moist Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10%
20 20 20 20 20 20 22 35.0 22	S7 3-16-44-51 (60)	24/24	• 0 ° • 0 ° 22.0 Bottor	imilar to S6 n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.

Lahlaf G	Geote	echnic		Billeri	helmsford F ca, MA 018 hone: 9783 9783305056	62 305912	BORING	BLOG B-4 PAGE 1 OF 1
	_			Solutions				ROJECT NAME: Prop. Manufacturing Building ROJECT LOCATION: Cranston, RI
DATE S BORING COORD SURFAG WEATH GROUN	G LC DINA CE I IER: IDW URI T EI	RTEI DCA1 ATES EI.: _ : _30 /ATE NG I NG I RC I	D: <u>12/2</u> FION: <u>N</u> : <u>NA</u> 58 ft. (s /s / Sunr R LEVEI DRILLING DF DRILL	1/22 Near SE corne see note 1)	r of prop.	building TOTAL DEP Based on sar	12/21/22	DRILLING SUBCONTRACTOR:Northern Drill Service, Inc. DRILLING FOREMAN:Tim Tucker DRILLING METHOD:Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL:Mobile B-53 ATV Rig HAMMER TYPE: _Automatic HAMMER WEIGHT:140 lb HAMMER DROP:30 in. SPLIT SPOON DIA:1.375 in. I.D., 2 in. O.D. CORE BARREL SIZE:NA LOGGED BY: _TG CHECKED BY: _NP
Depth (ff.) (ff.	l. .)	sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Strata	<u>Depth</u> El.(ft.)	Material Description
 5	_	0.5	S1 S2	14-12-8 (20) 9-10-6-4 (16) 4-3-2-2	18/14 24/15	Asphalt Fill	0.3 57.7 S1 - P trace o S2 - S	': Asphalt oorly Graded SAND with Silt (SP-SM), fine to medium, 10-15% fines, of organic soil, brown, moist imilar to S1 imilar to S1
	.0	6	S3	(5) 2-1-1-2 (2)	24/11 24/17		brown	ilty SAND (SM), fine to medium, 20-25% fines, trace of organic soil, , moist /ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, ~10%
<u>10</u> 		10	S5 S6	4-4-4-13 (8) 13-12-10-9 (22)	24/8 24/16	D	° ° ° ° ° ° ° S6 - S	/ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, ~10% 15-20% fine to coarse subangular gravel, light brown, moist imilar to S5, wet
<u>15</u> 	- - .0	15 17	S7	1-1-4-4 (5)	24/21	Sand and Gravel	wet	oorly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, gray,
20	-	20 22	S8	1-4-4-6 (8)	24/17		, o 22.0	/ell Graded SAND with Silt (SW-SM), fine to coarse, 5-10% fines, 10-15% coarse subangular gravel, light brown, wet
- <u>35.</u> - <u>-</u> 25 GENE I	_						Botton surfac	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.

Lahlaf Geotechn		Billeri Telep	Chelmsford R ca, MA 0186 hone: 97833 9783305056	2	BORING	BLOG B-S PAGE 1 OF		
						ROJECT NAME: Prop. Manufacturing Building		
LGCI PROJEC DATE STARTE BORING LOCA	D: <u>12/20</u>)/22			12/20/22	PROJECT LOCATION: _Cranston, RI DRILLING SUBCONTRACTOR: _Northern Drill Service, Inc. DRILLING FOREMAN: _Tim Tucker		
Coordinates Surface EI.: Veather: <u>3</u> Groundwati	<u>60 ft.</u> (se 0's / Sunn	ıy		TOTAL DEP	TH: <u>22 ft.</u>	DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb.		
	OF DRILLI	G: <u>15.0 ft. / E</u> ING: <u>14.0 ft.</u>			mple moisture	SPLIT SPOON DIA:: 1.375 in. I.D., 2 in. O.D. CORE BARREL SIZE: NA LOGGED BY: TG CHECKED BY: NP		
(ft.) (ft.) Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec.		Depth El.(ft.)	Material Description		
0.5-	S1	15-7-7 (14)	18/13	Asphalt	S1 - W fines, brick,	': Asphalt /ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% 15-20% fine to coarse subangular gravel, trace of organic soil, trace of brown, moist iece of brick		
+ - + - 4-	S2	5-4-6-5 (10)	24/1	Fill		/ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, ~10% 15-20% fine to coarse subangular gravel, light brown, moist		
<u>5 55.0</u> 6-	S3	6-3-3-4 (6)	24/11		S4 - S	ilty SAND (SM), fine to coarse, ~20% fines, 5-10% fine to coarse		
8-	S4	2-3-2-2 (5)	24/17		8.0 52.0 S5 - P	gúlar gravèl, tráce of organic soil, brown, moist oorly Graded SAND (SP), fine to medium, 0-5% fines, trace of fine , light brown, moist		
<u>50.0</u> 10-	S5	2-2-2-3 (4) 3-4-4-6	24/20	0	° S6-S	imilar to S5		
12- 	S6	(8)	24/18	0	°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°			
5 45.0 15- 17- 17-	S7	1-2-2-4 (4)	24/19	Sand and Gravel	S7 - S S7 - S S ⁰ S ⁰ C	andy SILT (ML), non-plastic, 30-35% fine to medium sand, gray, wet		
0 40.0 20-	S8	14-12-10-8 (22)	24/21	。 () 。 (S8 - W fines, 22.0	/ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% 15-20% fine to coarse subrounded gravel, brown, wet		
					Botton surfac	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.		
25 35.0 GENERAL NO								

Lahla	af Geo	otechn		Biller	Chelmsford F ica, MA 0180 bhone: 9783 9783305050	62 305912	BORING	BLOG B-6 PAGE 1 OF		
	-			t Solutions				PROJECT NAME: Prop. Manufacturing Building PROJECT LOCATION: Cranston, RI		
DATE BOR COO SURI WEA GRO QRO	E STA ING L RDIN FACE THEI UND DUF	ARTE LOCA IATE E EI.: R: <u>3</u> WAT RING END	ED: <u>12/2</u> ATION: <u>1</u> S: <u>NA</u> <u>60 ft. (: 0's / Sun</u> ER LEVE DRILLIN OF DRILL	-	prop. buil	TOTAL DEP	DRILLING SUBCONTRACTOR: _Northern Drill Service, Inc. DRILLING FOREMAN: _Tim Tucker DRILLING METHOD: _Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: _Mobile B-53 ATV Rig HAMMER TYPE: _Automatic HAMMER WEIGHT: _140 lb			
		HER:	- Sample	Blow Counts	Pen./Rec.	Y		LOGGED BY: TG CHECKED BY: NP		
(ff.)	(ft.)	Sample Interval (ft.)	Number	(N Value)	(in.)	원 Strata 산	Depth El.(ft.)	Material Description		
+	-	0.5	S1	5-8-6 (14)	18/18	Asphalt	S1 - S gravel	": Asphalt Silty SAND (SM), fine to medium, 20-25% fines, 5-10% fine subrounded I, trace of organic soil, trace of asphalt, brown, moist Vell Graded SAND with Silt (SW-SM), fine to coarse, 5-10% fines, 10-15°		
		4	S2	5-14-13-9 (27)	24/9		fine to	o coarse subrounded gravel, brown, moist		
5	55.0	6	S3	4-4-6-4 (10)	24/16	Fill		Similar to S2		
	_	8	S4	2-3-5-6 (8)	24/10		brown	Silty SAND (SM), fine to medium, 15-20% fines, trace of organic soil, n, moist		
10	50.0	10	S5	2-4-4-4 (8)	24/16	。 () 。 (S S S S S S S S S S S S S S S S S S S	Poorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, mois		
+		12	S6	4-5-5-6 (10)	24/17	° C	0 2°	Similar to S5, wet		
5	<u>45.0</u> 	15	S7	3-2-1-2 (3)	24/20		S7 - T fines, Bot. 1	op 10": Poorly Graded SAND with Silt (SP-SM), fine to medium, 10-15% brown, wet 0": Sandy SILT (ML), non-plastic, 30-35% fine sand, gray, wet		
20	+ -	20	S8	9-12-13-14 (25)	24/19	° (S8 - V fines, 22.0	Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% 15-20% fine subrounded gravel, brown, wet		
25							Bottor surfac	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.		

Lahlaf Geo		G (Consul	Billeri	helmsford R ca, MA 0186 hone: 97833 9783305056	2	BO	RING	BLOG B-7 PAGE 1 OF 1
-			Solutions					ROJECT NAME: Prop. Manufacturing Building ROJECT LOCATION: Cranston, RI
DATE STA BORING L COORDIN SURFACE WEATHEF GROUND	ARTED: LOCATIO IATES: E EI.: <u>6</u> R: <u>30's</u> WATER RING DR END OF	<u>12/2</u> DN: <u>N</u> <u>NA</u> <u>1 ft. (s</u> <u>/ Sunr</u> LEVEI RILLING	l/22 Jear western s see note 1)	ide of prop	b. building TOTAL DEP Based on sa	TH: _2	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc. DRILLING FOREMAN: Tim Tucker DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.) DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb. HAMMER WEIGHT: 1.375 in. I.D., 2 in. O.D. CORE BARREL SIZE: NA LOGGED BY: TG	
Depth (ff.) (ff.)		ample umber	Blow Counts (N Value)	Pen./Rec.	Strata	Depth El.(ft.)		Material Description
60.0		S1	2-6-8-6 (14)	24/8	Topsoil 30		S1 - S	ilty SAND (SM), fine to medium, 15-20% fines, trace of organic soil, trace halt, brown, moist
		S2	2-4-2-3 (6)	24/3				ilty SAND (SM), fine to coarse, ~20% fines, 5-10% fine to coarse unded gravel, trace of organic soil, trace of asphalt, black, moist
5		S3	5-6-3-5 (9)	24/6	Fill		S3 - S	imilar to S2
		S4	6-4-4-6 (8)	24/10			angula	Vell Graded GRAVEL with Silt and Sand (GW-GM), fine to coarse, ar, 10-15% fines, 25-30% fine to coarse sand, trace of organic soil, dark , moist
- <u> </u>		S5	5-4-2-5 (6)	24/9		10.0	S5 - S gray, r	ilty SAND (SM), fine to medium, 20-25% fines, 0-5% fine angular gravel, noist (appears reworked)
50.0		S6	7-3-3-5 (6)	24/14	. ()	51.0 5	S6 - P brown	oorly Graded SAND with Silt (SP-SM), fine to medium, 10-15% fines, , moist
		S7	4-8-8-15 (16)	24/8	, C	0 0		imilar to S6
		S8	9-9-8-41 (17)	24/19	Sand and Gravel		[⊻] S8 - S ¥	imilar to S6, wet
	20	S9	9-10-10-12 (20)	24/8	000	2°	S9 - W angula	Vell Graded GRAVEL with Silt and Sand (GW-GM), fine to coarse, ar, 5-10% fines, 20-25% fine to coarse sand, brown, wet
	22					0 22.0	Botton bags o	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings and four of sand.
25 GENERA		S:						

Lahlaf Geo	technic		Billeri	helmsford F ca, MA 0186 hone: 9783 9783305056	62 305912	BO	RING	ELOG B-E PAGE 1 OF
			Solutions				PF	ROJECT NAME: Prop. Manufacturing Building
GCI PRC	JECT	NUMBE	R: 2252				PF	COJECT LOCATION: Cranston, RI
DATE ST	ARTED): <u>12/19</u>	9/22	DATE C	OMPLETED:	12/19/	22	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.
BORING L	OCAT		lear eastern s	ide of prop	b. building			DRILLING FOREMAN:Tim Tucker
COORDIN								DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)
			ee note 1)		TOTAL DEP	TH: _22	2 ft	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig
VEATHEF GROUND							<u>.</u>	HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.
			.3. 3: <u>20.0 ft. / E</u>	1 43 0 ft	Rased on sa	nnle ma	nisture	SPLIT SPOON DIA: 1.375 in. I.D., 2 in. O.D.
			ING: <u>19.0 ft.</u>					CORE BARREL SIZE: NA
⊻ отн								LOGGED BY: TG CHECKED BY: NP
	e (ff.)				~			
ft.) EI. (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Strata	<u>Depth</u> El.(ft.)		Material Description
	0		2-3-5-10		Crushed Stone	0.3 62.7		op 3": Crushed stone
- -	2	X S1	(8)	24/11			trace c	: Poorly Graded SAND with Silt and Gravel (SP-SM), fine to medium, 6 fines, 15-20% fine to coarse subangular gravel, trace of organic soil, of brick, brown, moist poorly Graded SAND with Gravel (SP), fine to medium, 0-5% fines,
60.0		S2	7-8-7-5 (15)	24/14			15-20%	% fine to coarse subangular gravel, brown, moist
 5	4		6-7-6-7		Fill		S3 - P soil, tra	oorly Graded SAND (SP), fine to medium, 0-5% fines, trace of organic ace of brick, light brown, most
<u> </u>	6	X S3	(13)	24/19				
+ -		S4	5-5-5-8 (10)	24/18			S4 - S	milar to S3
55.0	8					8.0	S5 - P	oorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, moist
+ -		S5	4-5-5-5 (10)	24/19		S°.		
10	10+		(10)		。 〇	C		
			3-5-6-6	04/40	h -	0°.	56 - 5	milar to S5
Τ -		X S6	(11)	24/18	.0	C		
+ -	12				h 1	5° .		
50.0					• 0	d		
<u> </u>					b -	5°		
15					Sand and			
	15	/			Gravel 6	S°	S7 - S	milar to S5
+ -		X S7	3-6-9-4 (15)	24/17	00	0 U		
+ -	17				· (
45.0						C		
					• C	S.	_	
. † -						•	L	
20	20				• (Z S8 - S	milar to S5, wet
+ -		S8	2-6-5-15 (11)	24/18	0 0	4		
40.0	22	<u> </u>			• (22.0	Botton	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings.
25								
		ES:		· I	•			

Lahlaf Geotechnical Consulting,	100 Chelmsford Ro Billerica, MA 01862 Telephone: 97833 Fax: 9783305056		ORING LOG B-9 PAGE 1 OF 1
CLIENT: <u>Taco Comfort Solu</u> LGCI PROJECT NUMBER: 2			PROJECT NAME: Prop. Manufacturing Building
DATE STARTED: <u>12/19/22</u> BORING LOCATION: <u>Near v</u> COORDINATES: <u>NA</u> SURFACE EI.: <u>65 ft. (see n</u> WEATHER: <u>30's / Sunny</u> GROUNDWATER LEVELS:	DATE CO western side of prop ote 1)	. building TOTAL DEPTH: Based on sample	DRILLING FOREMAN: _Tim Tucker DRILLING METHOD: _Hollow Stem Auger (3-1/4" I.D.) 22 ft. DRILL RIG TYPE/MODEL: _Mobile B-53 ATV Rig HAMMER TYPE: _Automatic HAMMER WEIGHT: _140 lb HAMMER DROP: _30 in.
	w Counts Pen./Rec. Value) (in.)	Strata	epth .(ft.)
	6-12-11 (18) 24/15 5-3-4-2 (7) 24/16	Crushed 0 Stone 6	
5 60.0 6 S3 2	2-3-5-6 (8) 24/14	6.	S3 - Silty SAND (SM), fine to medium, 20-25% fines, 5-10% fine to coarse subrounded gravel, trace of organic soil, black, moist
S4 4 55.0 10	I-3-5-5 24/6		S4 - Poorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, moist
s5 3	3-5-6-7 (11) 24/17	Sand and Gravel	S5 - Similar to S4
17 17	10-10-10 (20) 24/18		S6 - Similar to S4 ▼
	10-15-17 (25) 24/24		
22 40.0 GENERAL NOTES:			Bottom of borehole at 22.0 feet. Borehole backfilled with drill cuttings.

Lahlaf Geo	otechn		Billeri	Chelmsford ica, MA 018 bhone: 978 978330505	862 33059		BOI	RING	LOG	B-10 PAGE 1 OF
			Solutions						OJECT NAME: Prop. Manufacturing Building	
LGCI PRO	OJEC		R : 2252					PF	OJECT LOCATION: Cranston, RI	
DATE ST	ARTE	ED: <u>12/1</u>	9/22	DATE C	COM	PLETED: _	12/19/2	22	DRILLING SUBCONTRACTOR: Northern Drill Se	ervice, Inc.
BORING	LOCA	ATION: _N	lear eastern s	ide of pro	op. bi	uilding			DRILLING FOREMAN: _ Tim Tucker	
COORDIN	IATE	S : <u>N</u> A							DRILLING METHOD: Hollow Stem Auger (3-1/4"	I.D.)
SURFACE	E EI.:	66 ft. (s	see note 1)		то	TAL DEPT	H: _21	ft.	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig	
NEATHE	R: _3	80's / Suni	ny						HAMMER TYPE: Automatic	
		ER LEVE							HAMMER WEIGHT: 140 lb. HAMMER D	ROP: 30 in.
			G: <u>19.0 ft. / E</u>				ple mo	isture	SPLIT SPOON DIA.: <u>1.375 in. I.D., 2 in. O.D.</u>	
₹ AT	END	OF DRILL	ING: Dry at	the end c	of dril	ling			CORE BARREL SIZE: NA	
⊻ оті	HER:	-							LOGGED BY: TG CHECKED B	BY: <u>NP</u>
EI. (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Remark	Strata	Depth El.(ft.)		Material Description	
	0	1			C	rushed	0.3		p 3": Crushed stone	
65.0		S1	6-7-6-5 (13)	24/15		Stone		Bot. 12 gravel,	": Silty SAND (SM), fine to medium, ~20% fines, 5- trace of asphalt, trace of brick, trace of organic soi	-10% fine subangular I, brown, moist
	2	S2	6-5-3-2 (8)	24/14		Fill		S2 - P 10-159	porly Graded SAND with Silt and Gravel (SP-SM), f 5 fines, trace of organic soil, light brown, moist	ine to medium,
5 60.0		S3	12-25-17-15 (42)	24/7				S3 - P fines, 2 moist	oorly Graded SAND with Silt and Gravel (SP-SM), f 5-30% fine to coarse angular gravel, trace of orgar	ine to medium, 5-109 nic soil, light brown,
	8	S4	37-36-30-23 (66)	24/16		· 0 ·		S4 - P 10-159	oorly Graded SAND with Silt and Gravel (SP-SM), f ofines, 25-30% fine to coarse angular gravel, light	ine to medium, brown, moist
0	9	S5	14-22-18-23 (40)	24/16		, 0 ° , 0 ° , 0 °		S5 - S	milar to S4	
	14	S6	8-7-3-3 (10)	24/14	Sa	and and Gravel		S6 - P 5-10%	oorly Graded SAND with Silt (SP-SM), fine to mediu fine to coarse subangular gravel, light brown, mois	um, 5-10% fines, t
20	- 19	S7	5-9-9-10 (18)	24/16			c ź	S7 - S	milar to S6, wet	
	- 21							Botton	of borehole at 21.0 feet. Borehole backfilled with o	Irill cuttings.

Lahlaf Geo	otechn		Billeri	Chelmsford F ica, MA 018 hone: 9783 9783305056	62 305912	BO	RING	BLOG B-11 PAGE 1 OF 1				
-			t Solutions					ROJECT NAME: Prop. Manufacturing Building				
LGCI PRO	DJEC		ER: 2252				ROJECT LOCATION: Cranston, RI					
			9/22			12/19/	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.					
			Near NE corne	r of prop.	building		DRILLING FOREMAN: _Tim Tucker					
COORDIN							DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)					
			see note 1)		TOTAL DEI	PTH: <u>22</u>	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig					
WEATHEI GROUND												
			:LS: IG: _Not encou	intered				HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in. SPLIT SPOON DIA: 1.375 in. l.D., 2 in. O.D.				
			LING: Dry at 1		f drilling			CORE BARREL SIZE: NA				
⊥ ⊥ Ω I I I I I I I I I I I I I			LING. Diyat		unning			LOGGED BY: TG CHECKED BY: NP				
		-										
Depth (ft.) (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Strata	Depth El.(ft.)		Material Description				
	0	Ν/			Crushed Stone	0.5	S1 - T	op 6": Crushed stone				
- + -	2	S1	6-10-11-11 (21)	24/14	stone	67.5	to coa	': Silty SAND with Gravel (SM), fine to coarse, 20-25% fines, 15-20% fine rse subangular gravel, trace of organic soil, trace of asphalt, brown, moist				
65.0		S2	14-14-15-12 (29)	24/8	Fill		fines.	S2 - Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% fines, 25-30% fine to coarse angular gravel, trace of organic soil, trace of asphalt, brown, moist				
	4	S3	15-19-19-18 (38)	24/15			S3 - S	- Similar to S2, black				
- + -	6	$\left(\right)$				6.5	S4 - T	op 6": Similar to S2, black				
60.0		S4	14-13-12-12 (25)	24/17	0	0°	Bot. 1 5-10%	1": Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse, fines, ~15% fine to coarse subrounded gravel, light brown, moist				
	8.	S5	10-8-8-8 (16)	24/16	。)	• 0 • 1	S5 - P brown	oorly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, light , moist				
	10	S6	9-12-10-13 (22)	24/17	。)	2 C 0° 0	S6 - S	imilar to S5				
- <u>- 55.0</u> - <u></u> - 15	12				Sand and	0°	• • •					
	-	S7	4-6-6-7 (12)	24/16		0° 2 C 0°	S7 - S	imilar to S5				
50.0	20											
	20	S8	11-10-8-8 (18)	24/19			S8 - S	imilar to S5				
45.0	22						Botton	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings.				
25												
GENERA	L NC	DTES:										

Lahlaf Geo	otechn		Billeri	helmsford R ca, MA 0186 hone: 97833 9783305056	62 305912	BO	RING	BLOG B-12 PAGE 1 OF 1			
			t Solutions					ROJECT NAME: Prop. Manufacturing Building			
LGCI PRO	DJEC		R : 2252				PF	ROJECT LOCATION: Cranston, RI			
DATE ST	ARTE	D: <u>12/2</u>	0/22	DATE CO	OMPLETED	D: <u>12/20/</u>	22	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.			
BORING	LOCA		Vear western s	ide of pro	p. building			DRILLING FOREMAN: Tim Tucker			
COORDIN	ATE	S: <u>NA</u>					DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)				
SURFAC	E EI.:	_66 ft. (s	see note 1)		TOTAL DE	EPTH: _22	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig				
WEATHE	R: _3	0's / Sun	ny				HAMMER TYPE: Automatic				
GROUND							HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.				
			G: <u>20.0 ft. / E</u>			sample mo	oisture	SPLIT SPOON DIA.:1.375 in. I.D., 2 in. O.D.			
TA 🐺	END	OF DRILL	LING: Dry at t	the end of	drilling			CORE BARREL SIZE: NA			
ТО ⊈	HER:	-						LOGGED BY: TG CHECKED BY: NP			
Depth (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	E Strata	a Depth El.(ft.)		Material Description			
05.0	0.5				Asphalt	0.3 65.7	<u>Top 3"</u>	": Asphalt			
65.0	2	S1	14-16-13 (29)	18/13	Fill	2.0	coarse	illty SAND with Gravel (SM), fine to coarse, ~15% fines, 15-20% fine to e subangular gravel, trace of organic soil, trace of brick, light brown, moist			
- + -		S2	10-10-12-9 (22)	24/15			S2 - W fines,	Vell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 15-20% fine to coarse subangular gravel, light brown, moist			
5	- 4	S3	5-7-10-10 (17)	24/16	2	° ° °	S3 - P	oorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, moist			
60.0	- 6	S4	4-5-7-8 (12)	24/18	D	, 0 ° 0 ° 0 °	S4 - Similar to S3				
	- 10 - 12	S5	5-8-6-8 (14)	24/18	Sand and Gravel	ο C ο C ο C ο C ο C ο C ο C ο C		imilar to S3, fine to medium, trace coarse			
	- 15- - 17-	S6	5-11-6-8 (17)	24/16			S6 - P brown	oorly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, light , moist			
	20-	s7	5-9-9-10 (18)	24/15		~ ~	Botton	imilar to S6, wet n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground			
 25 GENERA		DTES:					surfac	e restored with asphalt cold patch.			

Lahla	f Geo	otechni		Billeri	Chelmsford ca, MA 018 hone: 9783 978330505	362 3305		BO	RING	LOG B-13 PAGE 1 OF 1		
	-			t Solutions						ROJECT NAME: Prop. Manufacturing Building		
LGCI	PRO	JEC.	T NUMBE	R : 2252					PF	OJECT LOCATION: Cranston, RI		
DATE	ST/	ARTE	D: <u>12/2</u>	0/22	DATE C	CON	APLETED: _	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.				
				Near NW corne	er of prop). bi	uilding	DRILLING FOREMAN: _Tim Tucker				
			S: <u>NA</u>					DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)				
				see note 1)		T	OTAL DEPT	2 ft	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig			
			<u>0's / Sun</u>							HAMMER TYPE: Automatic		
	-			-		_				HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.		
				G: <u>20.0 ft. / E</u> L ING: <u>Dry at f</u>				pie mo	Disture	SPLIT SPOON DIA.: 1.375 in. I.D., 2 in. O.D. CORE BARREL SIZE: NA		
		IER:		LING: Dry at	ine end d		ming			LOGGED BY: TG CHECKED BY: NP		
<u>+</u>	011		-	I	1							
	El. (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Remark	Strata	<u>Depth</u> El.(ft.)		Material Description		
		0	1				Topsoil	1 0.2 66.8		opsoil		
- +	-		X S1	5-6-6-5 (12)	24/2			2				
	65.0	2-	Δ				Fill		00.14			
			\mathbb{N}	4-5-7-14	0.4/5				angula	ell Graded GRAVEL with Silt and Sand (GW-GM), fine to coarse, r, 5-10% fines, 15-20% fine to coarse sand, trace of organic soil, brown,		
	_	1	S2	(12)	24/5				moist			
- +	_	4-	$\left(\right)$			┥┝	•	4.0 63.0	S3 - W	ell Graded SAND with Silt (SW-SM), fine to coarse, 5-10% fines, 10-15%		
5	_		X s3	10-12-10-9	24/13		· 0 ·		fine to	coarse subangular gravel, brown, moist		
				(22)				d				
	-	6-					· 0 ·		S4 - Si	milar to S3		
	60.0		X S4	10-9-9-10 (18)	24/12							
\downarrow \downarrow	_	8-	/ N	. ,			° 0 °					
							200					
- +	-	İ					· 0 ·	° C				
_10	-	10-	1				Poc	>	S5 - Si	milar to S3		
	_		X S5	7-10-9-8	24/16		· 0 ·	, C				
	55.0		\mathbb{N}^{-1}	(19)								
		12-					0	d				
- +	_						Sand and • 🗅 Sand and					
	_							d				
15							· 0 ·	,				
	-	15-	1					, C	S6 - P	porly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, light		
- +	_		X S6	11-10-8-12 (18)	24/17		° 0 °		brown,	moist		
	50.0	17-	$\langle \rangle$	(10)								
							• O '	, ,				
\vdash $+$	_						200					
\vdash \downarrow	_						le la	, C				
20		20							₽			
	_	20-	$\overline{\Lambda}$	0 40 47 47]	0 0	d	S7 - S	milar to S6, wet		
\vdash $+$	_		X S7	8-12-17-17 (29)	24/18		° 0 °					
╞╶┼	45.0_	22-	<u>/ </u>			┤┝		22.0	Botto~	of horobolo at 22.0 foot Borobolo bookfilled with drill outtings		
									DOILON	of borehole at 22.0 feet. Borehole backfilled with drill cuttings.		
ΓŤ	_											
\vdash $+$	_											
25												
GEN	IERA		TES:									

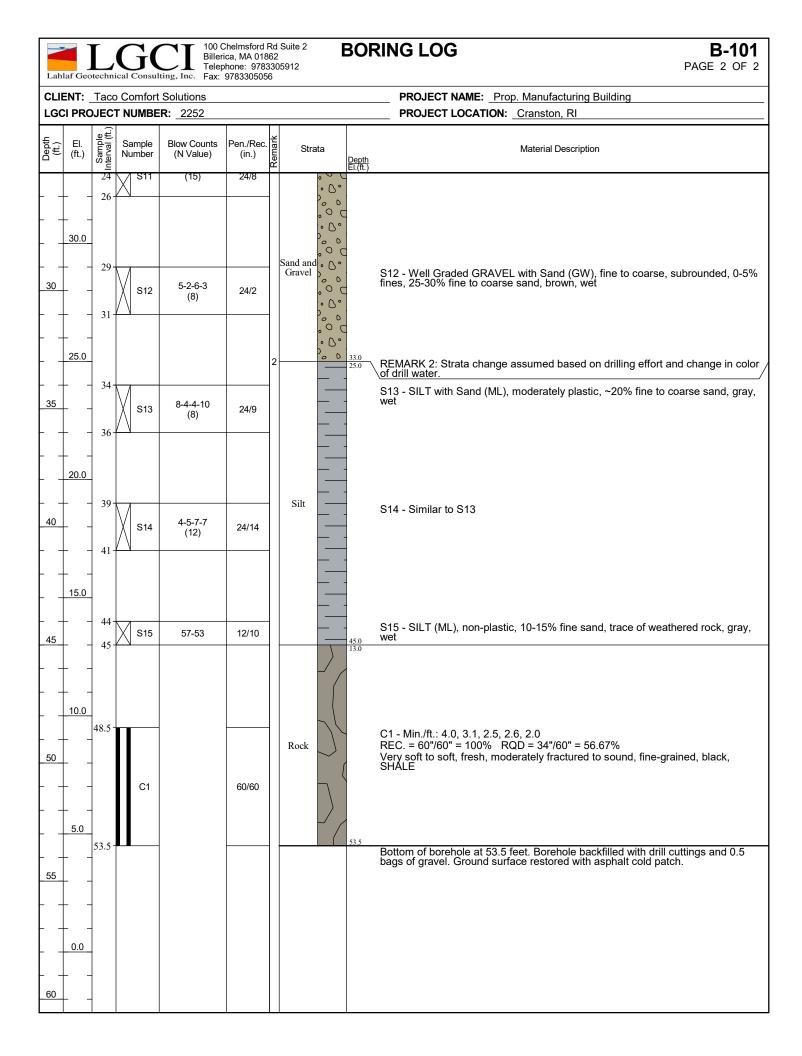
Lahlaf Geotechnical Consulting, Inc. 100 Chelmsford Rd Suite 2 Billerica, MA 01862 Telephone: 9783305912 Fax: 9783305056										ORING LOG B-14 PAGE 1 OF 1				
CLIE	NT:	Taco	o Comfor	t Solutions					PR	ROJECT NAME: Prop. Manufacturing Building				
LGCI	I PRC)JEC	t numbe	ER: <u>2252</u>					PR	ROJECT LOCATION: Cranston, RI				
BOR	ING L			9/22 Near NE corne				DRILLING SUBCONTRACTOR: Northern Drill Service, Inc. DRILLING FOREMAN: Tim Tucker						
			S: <u>NA</u>					DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)						
				see note 1)		TOTAL	DEPTH	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig						
			<u>0's / Sun</u> E R LEVE	-				<u>.</u>	HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.					
	-			G: <u>22.0 ft. / E</u>	I. 46.0 ft.	Based o	on samp	sture	SPLIT SPOON DIA: 1.375 in. I.D., 2 in. O.D.					
				LING: Dry at t						CORE BARREL SIZE: NA				
	OTH			-		-				LOGGED BY: TG CHECKED BY: NP				
Depth (ft.)	El.	nple /al (ft.)	Sample	Blow Counts	Pen./Rec. (in.)	ark S	irata			Material Description				
ă.	(ft.)	Sample Interval (Number	(N Value)	(in.)	Ren		Depth El.(ft.)						
		0.5-				Aspha		0.3		": Asphalt				
- +		2-	S1	16-20-10 (30)	18/16				fines, 2 brick, t	Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% 20-25% fine to coarse subangular gravel, trace of organic soil, trace of trace of asphalt, brown, moist				
	65.0		S2	20-16-18-13 (34)	24/12	Fill		4.0	S2 - W fines, 2	Nell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 20-25% fine to coarse subangular gravel, light brown, moist				
5		4	S3	7-15-16-20 (31)	24/13		· C ·	64.0	S3 - W fines, 2	Nell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 25-30% fine to coarse angular gravel, light brown, moist				
	 	8-	S4	18-17-16-14 (33)	24/15				S4 - Si	Similar to S3				
	 55.0	10-	\$5	11-14-15-13 (29)	24/21	Sanda	, 0 , 0 , 0 , 0 , 0 , 0 , 0 , 0 , 0 , 0		S5 - Po	Poorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, mois				
	 50.0	- 15- - 17-	S6	12-14-11-9 (25)	24/18	Grave		-	S6 - W fine to	Well Graded SAND with Gravel (SW), fine to coarse, 0-5% fines, 15-20% o coarse subrounded gravel, light brown, moist				
	 	20-	S7	9-17-18-15 (35)	24/21				subrou	Poorly Graded SAND (SP), fine to medium, 0-5% fines, 5-10% fine nunded gravel, light brown, moist to wet m of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground				
	45.0 		DTES:						surface	ce restored with asphalt cold patch.				

Lahlaf Geo	otechr		Billeri	Chelmsford R ca, MA 0186 hone: 9783 9783305056	62 305912	BOF	RING	ELOG B-15 PAGE 1 OF 1				
CLIENT:	Tac	o Comfor	t Solutions				PR	ROJECT NAME: Prop. Manufacturing Building				
LGCI PRO	OJEC		ER: 2252				PR	ROJECT LOCATION: Cranston, RI				
DATE ST	ARTE	ED: <u>12/2</u>	1/22	DATE C	OMPLETED	12/21/2	22	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.				
			Near SW corne	er of prop.	building		DRILLING FOREMAN: _Tim Tucker					
COORDIN							DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)					
			see note 1)		TOTAL DE	PTH: <u>22</u>	<u>ft.</u>	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig				
WEATHE												
			G: <u>15.0 ft. / E</u>	1 44 0 ft	Poord on o	molo moi	iatura	HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in. SPLIT SPOON DIA.: 1.375 in. I.D., 2 in. O.D.				
			LING: 13.0 ft.					CORE BARREL SIZE: NA				
То 🖞			<u></u>	/ []. 40.0	1			LOGGED BY: TG CHECKED BY: NP				
Depth (ft.) (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. • (in.)	Strata	Depth El.(ft.)		Material Description				
	0.5				Asphalt	0.3		: Asphalt /ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10%				
	2	S1	18-13-5 (18)	18/14			fines, 1	15-20% fine to coarse subrounded gravel, light brown, moist				
		\mathbb{N}	8-11-14-11	0.1/0			52 - No	o recovery				
	1	S2	(25)	24/0								
55.0	4	$\left\{ \right\}$					S3 - W	/ell Graded SAND (SW), fine to coarse, 0-5% fines, 5-10% fine				
	-	S3	5-5-4-5 (9)	24/17	Fill		subrounded gravel, light browń, moist					
- + -	6	$\left\{ \right\}$					S4 - Si	imilar to S3				
	-	X S4	6-8-7-4 (15)	24/17								
	8	\mathbb{N}	(10)									
50.0	0											
	1											
	10	1				10.4	S5 - To	op 5": Silty SAND (SM), fine to medium, 25-30% fines, trace of organic				
		X S5	1-1-13-17	24/21	0	0°	∖ <u>soil, br</u>	rown, moist				
		\mathbb{N}^{\sim}	(14)		0	D	Bot. 16 light br	S": Poorly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, rown, moist				
- + -	12				l l	D C	•					
	-				0	°° ₹						
45.0					0	ρc						
15					b	0° 7						
	15	M			0	ວັດ 🍈	S6 - W	/ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 20-25% fine to coarse angular gravel, brown, wet				
- + -	-	X S6	10-10-11-30 (21)	24/8	Ground	0°	11165, 2	20-23 % fille to coarse angular graver, brown, wet				
	17	<u> </u>			0	D C						
	-				0	0°]						
	1				0	o C						
40.0	1				0	0.						
_20	20	\downarrow			Po	D	07 14					
		\mathbb{N}	2-4-11-21	04/40	P P	0° 0°	S7 - W fine su	/ell Graded SAND with Silt (SW-SM), fine to coarse, 5-10% fines, 5-10% brounded gravel, brown, wet				
	1	S7	(15)	24/19	Po	D						
+ ·	22	<u>v v</u>					Bottom	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings. Ground e restored with asphalt cold patch.				
F + -	1						Sunaut					
35.0	-											
25												
GENER/	AL NO	DTES:										

Billerica, I	msford Rd Suite 2 MA 01862 e: 9783305912 3305056	LOG B-16 PAGE 1 OF 1
CLIENT: Taco Comfort Solutions		OJECT NAME: Prop. Manufacturing Building
LGCI PROJECT NUMBER: 2252 DATE STARTED: 12/22/22 DA	PR(DJECT LOCATION: Cranston, RI DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.
BORING LOCATION: <u>Near SE corner of</u> COORDINATES: NA	f prop. parking lot	DRILLING FOREMAN: <u>Tim Tucker</u> DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)
SURFACE EI.: <u>56 ft.</u> (see note 1)	TOTAL DEPTH: <u>12 ft.</u>	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig
WEATHER: _40's / Sunny		HAMMER TYPE: Automatic
GROUNDWATER LEVELS:	16.0 ft. Based on sample moisture	HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in. SPLIT SPOON DIA: 1.375 in. l.D., 2 in. O.D.
AT END OF DRILLING: Dry at the		CORE BARREL SIZE: NA
⊻ OTHER:		LOGGED BY: TG CHECKED BY: NP
	(in.)	Material Description
55.0 0.5	Asphalt 0.4 Top 5":	Asphalt ty SAND (SM), fine to coarse, 15-20% fines, 5-10% fine to coarse ular gravel, trace of organic soil, trace of asphalt, brown, moist
S1 11-7-4 1	18/16 subang	úlar gravèl, tráce of organic sóil, trace of asphalt, brown, moist
$ 2$ \times $ 2$ \times $ 2$ \times $ -$	24/15 S2 - Sil gravel,	ty SAND (SM), fine to medium, 15-20% fines, 0-5% fine subrounded trace of organic soil, brown, moist
- $ +$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$		nilar to S2, trace of asphalt
- <u>50.0</u> 6 S4 <u>1-2-3-9</u> 2	6.8	p 9": Similar to S2, trace of asphalt Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse.
	P _ 6	Well Graded SAND with Silt and Gravel (SW-SM), fine to coarse, fines, 20-25% fine to coarse subangular gravel, light brown, moist
S5 17-16-19-22 (35) 2	24/16 Sand and $\circ \circ \circ$ Gravel 2	nilar to S4 Bot. 8"
	24/12	ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 10-15% 0-35% fine to coarse angular gravel, gray, wet
	Bottom surface	of borehole at 12.0 feet. Borehole backfilled with drill cuttings. Ground restored with asphalt cold patch.
15		
40.0		
20		
35.0		
25 GENERAL NOTES:		

Lahlaf Geotechr		Billeri	helmsford F ca, MA 018 hone: 9783 978330505	62 3305912	BO	RING	LOG B-17 PAGE 1 OF 1		
CLIENT: Tac	o Comfort	Solutions				PF	ROJECT NAME: Prop. Manufacturing Building		
LGCI PROJEC		R : 2252				PF	OJECT LOCATION: Cranston, RI		
DATE START	ED: <u>12/2</u>	2/22	DATE C	OMPLETE	D: <u>12/22/</u>	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.			
BORING LOC	ATION: _N	lear center of	prop. buil	ding		DRILLING FOREMAN: _ Tim Tucker			
COORDINATE						DRILLING METHOD: Hollow Stem Auger (3-1/4" I.D.)			
SURFACE EI.:				TOTAL D	EPTH: _22	tt.	DRILL RIG TYPE/MODEL: Mobile B-53 ATV Rig		
WEATHER: _3		1					HAMMER TYPE: Automatic		
		-					HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.		
		G: <u>20.0 ft. / E</u>			sample mo	oisture	SPLIT SPOON DIA.: <u>1.375 in. I.D., 2 in. O.D.</u>		
$\underline{\Psi}$ at end $\underline{\Psi}$ other:		ING: Dry at t	the end of	t drilling					
		1	1				LOGGED BY: TG CHECKED BY: NP		
Depth (ft.) (ft.) (tub) Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Strata	a <u>Depth</u> El.(ft.)		Material Description		
				Crushed	0.3		op 3": Crushed stone		
60.0	S1	11-34-20-12 (54)	24/10	stone		to coa moist	: Silty SAND with Gravel (SM), fine to coarse, 15-20% fines, 20-25% fine se angular gravel, trace of organic soil, trace of roots, orange-brown,		
	S2	5-11-19-12 (30)	24/16	¹ Fill		feet ar	RK 1: Encountered possible abandoned foundation between depths of 2 d 4 feet. ece of concrete		
5 4	S3	13-13-10-9 (23)	24/10	h b		S3 - W fines, 2	ell Graded SAND with Silt and Gravel (SW-SM), fine to coarse, 5-10% 20-25% fine to coarse angular gravel, light brown, moist		
- <u>55.0</u> 6 8	S4	18-13-15-16 (28)	24/24	• •	· 0 ° • 0 °	S4 - P 10-159	oorly Graded SAND (SP), fine to medium, trace coarse, 0-5% fines, % fine to coarse subangular gravel, light brown, moist		
$\frac{10}{50.0}$ 10	S5	5-7-5-6 (12)	24/20	• • •		S5 - P fine su	oorly Graded SAND (SP), fine to medium, trace coarse, 0-5% fines, ~5% brounded gravel, light brown, moist		
15 - 15 45.0 - 17	S6	10-6-5-5 (11)	24/16	Gravel D		S6 - S	milar to S5		
20 - 20 40.0 - 22	S7	3-4-5-7 (9)	24/24				milar to S6		
25 GENERAL NO						BOLLON	n of borehole at 22.0 feet. Borehole backfilled with drill cuttings.		

Lahlaf Geo	Detechn	G	Billeri	Chelmsford I ica, MA 018 ihone: 9783 978330505	362 3305		E	BORING	B-101 PAGE 1 OF 2		
			rt Solutions ER: 2252						ROJECT NAME: Prop. Manufacturing Building ROJECT LOCATION: Cranston, RI		
DATE STA BORING I COORDIN SURFACE WEATHEI GROUND	ARTE LOCA NATE E EI.: R: <u>5</u> WAT RING END	ED: <u>2/1</u> ATION: <u></u> S: <u>NA</u> <u>58 ft.</u> <u>0's / Clo</u> ER LEVI DRILLII OF DRIL	7/23 Near southern (see note 1) udy	. 50.0 ft. E	rop. T(Bas	building DTAL DI	EPTH	/17/23	DRILLING SUBCONTRACTOR: Northern Drill Service, Inc. DRILLING FOREMAN: Jon Beirholm DRILLING METHOD: Drive and wash with 4-inch casing DRILL RIG TYPE/MODEL: Mobile B-48 ATV Rig HAMMER TYPE: Automatic HAMMER WEIGHT: 140 lb. HAMMER WEIGHT: 1.375 in. I.D., 2 in. O.D. CORE BARREL SIZE: NX LOGGED BY: TG		
Depth (ft.) (ft.)	Sample Interval (ft.)	Sample Number		Pen./Rec. (in.)	Remark	Strat		<u>Depth</u> EI.(ft.)	Material Description		
	0.5	S1	8-5-8 (13)	18/2		<u>Asphalt</u>		0.3 57.7 S1 - P 5-10% moist	: Asphalt oorly Graded SAND with Silt (SP-SM), fine to medium, trace coarse, fines, ~10% fine angular gravel, trace of asphalt, trace of brick, brown, oorly Graded SAND (SP), fine to medium, 0-5% fines, light brown, moist		
<u>55.0</u> 	- 4-	S2 S3	12-6-4-3 (10) 6-6-7-6 (13)	24/12	1	Fill		REMARK 1: Organic soil washing up in drill cuttings at depth of 3 feet. S3 - Poorly Graded SAND with Silt (SP-SM), fine to medium, trace coarse, 5-10% fines, 5-10% fine subrounded gravel, brown, moist (appears reworked)			
 _ <u>50.0</u>	- 6-	S4	7-5-4-2 (9)	24/11				V	imilar to S3 ilty SAND (SM), fine to coarse, 20-25% fines, 0-5% fine subrounded		
	- 10-	S5	2-1-2-2 (3) 12-11-10-11	24/6				gravel	trace of organic soil, brown, wet op 6": Similar to S5, 15-20% fines ': Poorly Graded SAND with Silt (SP-SM), fine to medium, 10-15% fines,		
	- 12-	S6	8-7-9-12 (16)	24/14				orange	e-brown, wet oorly Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines,		
	- 14-	S8	17-25-17-12 (42)	24/7				S8 - P coarse	oorly Graded SAND with Silt and Gravel (SP-SM), fine to medium, trace 9, 5-10% fines, 20-25% fine to coarse angular gravel, brown, wet		
 40.0	- 16· - 18·	S9	16-9-10-15 (19)	24/4		Sand and Gravel			imilar to S8, ~15% fine to coarse angular gravel		
	- 19-	S10	10-10-9-7 (19)	24/2				S10 - I 5-10%	Poorly Graded SAND with Silt (SP-SM), fine to medium, trace coarse, fines, 10-15% fine to coarse subangular gravel, light brown, wet		
<u>35.0</u> 	- 24-		8-7-8-6		-				Similar to S10, 0-5% fine subrounded gravel		



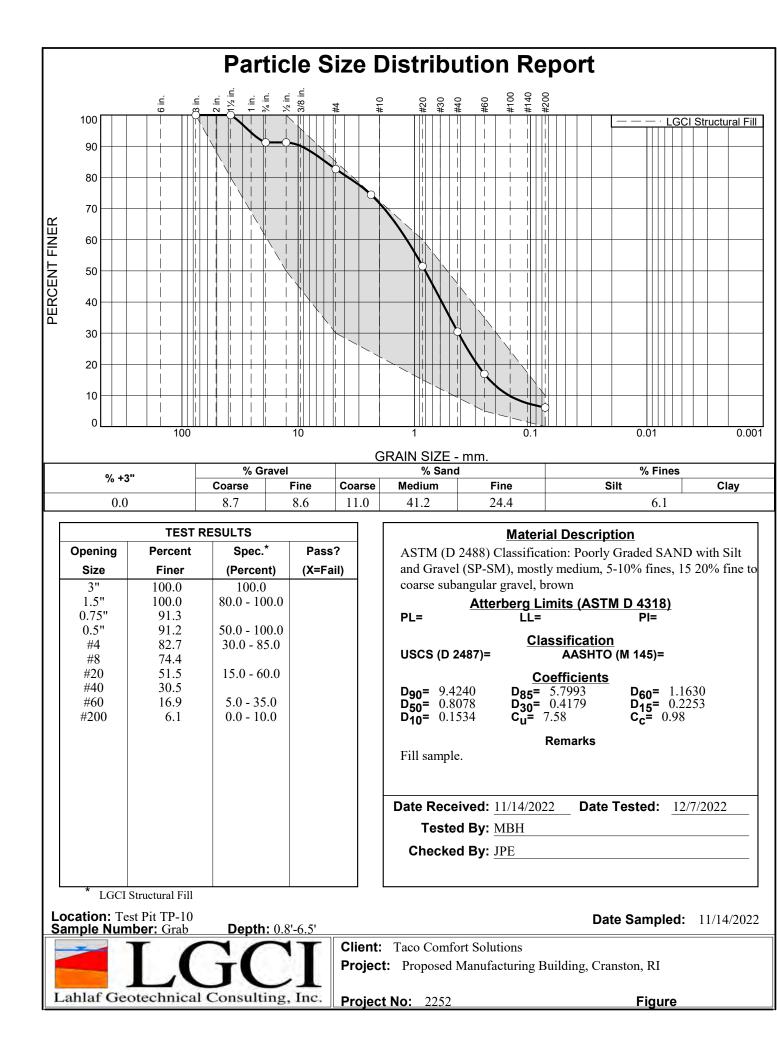
Lablaf Geotechnical Consulting, Inc.100 Chelmsford Rd Suite 2 Billerica, MA 01862 Telephone: 9783305056BORING LOGB-102 PAGE 1 OF 2									
							ROJECT NAME: Prop. Manufacturing Building		
LGCI PROJECT NUMBER: 2252 PF							ROJECT LOCATION: Cranston, RI		
DATE STARTED: 2/20/23 DATE COMPLETED: 2/20/23							DRILLING SUBCONTRACTOR: Northern Drill Service, Inc.		
BORING LOCATION: Near SE corner of prop. building							_ DRILLING FOREMAN: _Jon Beirholm		
COORDINATES: NA							DRILLING METHOD: Drive and wash with 4-inch casing		
SURFACE EI.: 57 ft. (see note 1) TOTAL DEPTH: 49 ft.							DRILL RIG TYPE/MODEL: Mobile B-48 ATV Rig		
WEATHER: _50's / Cloudy							HAMMER TYPE: _Automatic		
GROUNDWATER LEVELS:							HAMMER WEIGHT: 140 lb. HAMMER DROP: 30 in.		
URING DRILLING: <u>6.0 ft. / El. 51.0 ft. Based on sample moisture</u>						sample mois	SPLIT SPOON DIA.: <u>1.375 in. I.D., 2 in. O.D.</u>		
	▲ AT END OF DRILLING: <u>8.0 ft. / El. 49.0 ft.</u> ✓ OTHER:								
<u><u></u> <u></u> <u></u> <u></u></u>	IER:	-					LOGGED BY: <u>NP</u> CHECKED BY: <u>TG</u>		
Depth (ft.)	Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Stra Kemark	ta <u>Depth</u> El.(ft.)		Material Description	
	0.5				Asphalt		_ Top 3"	: Asphalt	
55.0		S1	14-10-12 (22)	18/13			S1 - Po fine su	porty Graded SAND with Silt (SP-SM), fine to medium, 5-10% fines, 0-5% brounded gravel, trace of asphalt, brown, moist	
	2	М	10-10-8-6				S2 - Si	milar to S1, trace of organic soil, no asphalt	
- + -		X S2	(18)	24/16					
- + -	4	$\left(\right)$			Fill		63 N	o recovery	
5		X S3	8-7-10-8	24/0			00-14		
		\mathbb{N}^{33}	(17)	24/0					
- + -	6	$\left(\right)$			-		Z S4 - Po	porly Graded SAND (SP), fine, 0-5% fines, light brown, wet	
50.0		X S4	12-7-9-7	24/17					
		\mathbb{N}	(16)			8.0	,		
	8	M			Buried	49.0	S5 - Si	Ity SAND (SM), fine to medium, 25-30% fines, trace of organic soil, trace s, black, wet	
- + -		X 85	4-4-6-9 (10)	24/22	Organic Soil	\sim	011001	S, DIAUN, WEL	
_10	10	$\left\{ \right\}$			501	10.0	00 D	and Craded CAND with Cill (CD CN), fine to medium 40.450/ fines	
		\mathbb{N}	6-6-7-7			47.0	trace c	porly Graded SAND with Silt (SP-SM), fine to medium, 10-15% fines, forganic soil, trace of roots, brown, wet	
	1	S6	(13)	24/12	Fill				
45.0	12	()				45.0	S7 - Sa	andy SILT (ML), non-plastic, 40-45% fine sand, light brown, wet	
		X S7	1-2-1-1	24/13					
		$ \rangle$	(3)						
[† -	14	M					S8 - Si	milar to S7	
		X S8	1-2-2-2 (4)	24/7	Silt				
$\downarrow \downarrow$ -	16	μ							
40.0									
	1				1	17.5		RK 1: Strata change assumed.	
F + -						• 0 • 3 9.5			
$\downarrow \downarrow$ -	19-					00	0		
20		M	10-9-11-8			• 0 °	S9 - Po coarse	porly Graded SAND with Silt and Gravel (SP-SM), fine to medium, trace , 10-15% fines, 20-25% fine to coarse subangular gravel, light brown, wet	
	1	S9	(20)	24/11		00			
┣ ┿ -	21	۲ N			Sand and	. O C			
35.0					Gravel	• 0 ° • 0			
						°° C			
+ -	1					° D°			
	24	k				0 C	S10 - 9	Similar to S9, 5-10% fines	
25		\square	16-9-10-10			° O °	010-0		
GENERA	GENERAL NOTES:								

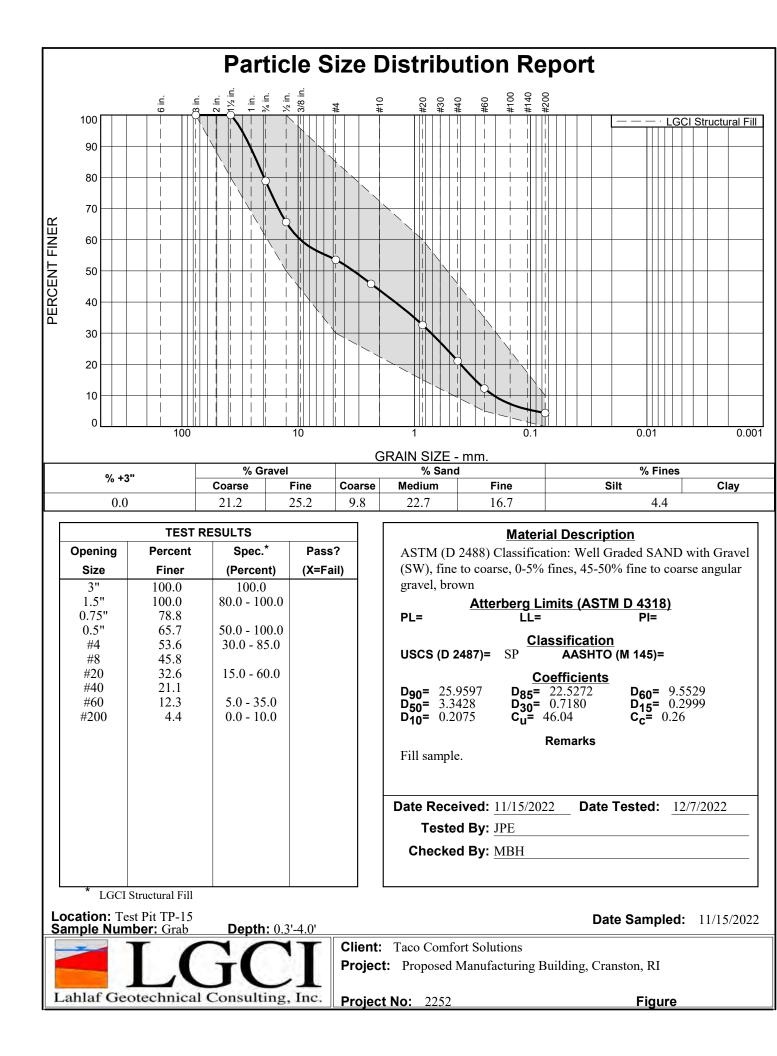
GENERAL NOTES:

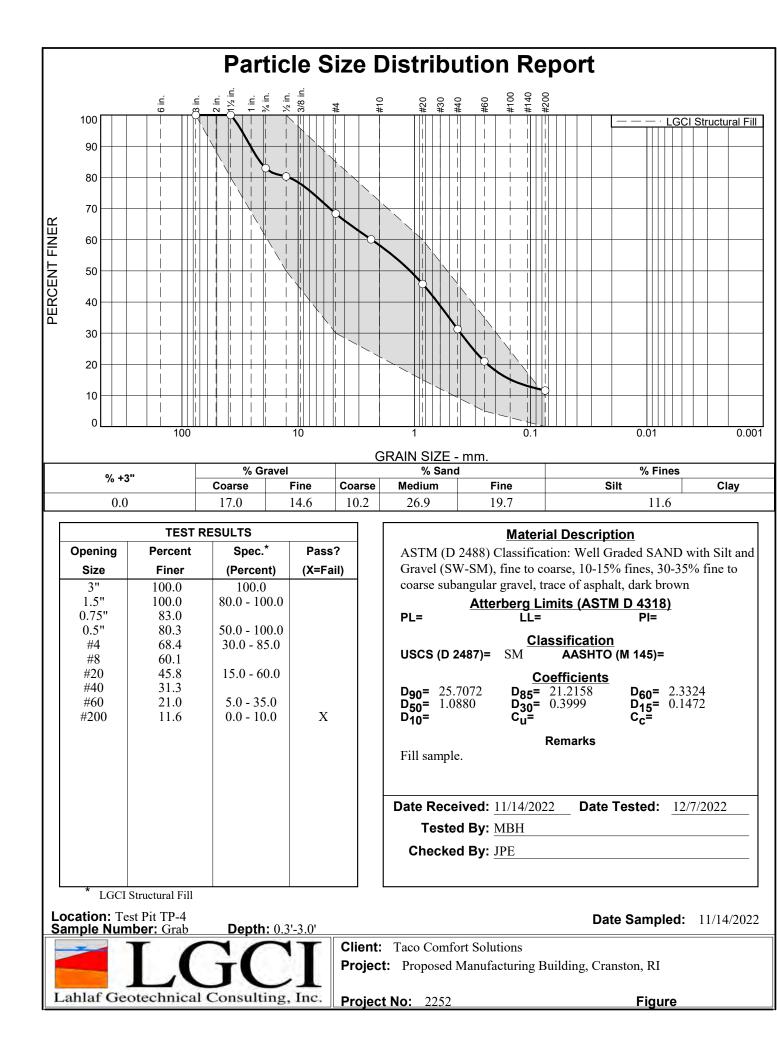
1. The ground surface elevation was interpolated to the nearest foot from drawing C-200 titled: "Civil Proposed Site Plan," prepared by Woodard & Curran, dated August 2022, and provided to LGCI by Thermo-Mechanical Systems Corporation via e-mail on August 23, 2022.

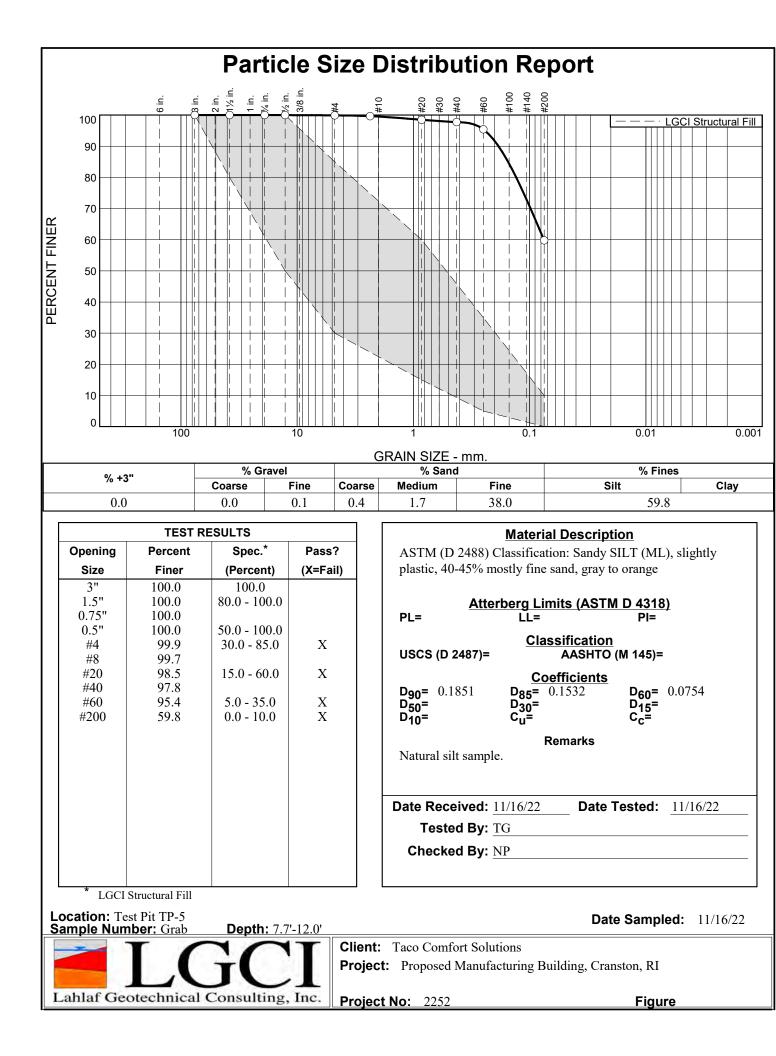
Lahlaf Geotechnical Consulting, Inc. Lahlaf Geotechnical Consulting, Inc. Billerica, MA 01862 Telephone: 9783305056 Fax: 9783305056 BORING LOG BORING LOG PAGE 2 OF 2								
CLIENT: Taco Comfort Solutions PROJECT NAME: Prop. Manufacturing Building LGCI PROJECT NUMBER: 2252 PROJECT LOCATION: Cranston, RI								
				×				
Depth (ft.) (ft.) :TJ :TI Sample Interval (ft.)	Sample Number	Blow Counts (N Value)	Pen./Rec. (in.)	Strata	Material Description Depth El.(ft.)			
26-	S10	(19)	24/18	° 0 °	4			
30.0 30.0 29. 30 31	S11	6-7-8-7 (15)	24/15	Sand and Gravel	 S11 - Poorly Graded SAND with Silt and Gravel (SP-SM), fine to medium, trace coarse, 5-10% fines, ~20% fine to coarse subrounded gravel, light brown, wet 			
25.0 34 35	Mara	3-4-3-4		° 0°				
20.0 20.0	S12	(7)	24/22	Silt				
40 39 40 41 41	S13	6-5-13-11 (18)	24/20	Sand and O				
44 ⁻	S14	61-36-64/4" (100/10")	16/12	° 0 °	•			
45.3				2 Rock Rock	46.0 11.0 REMARK 2: Drill bit refusal encountered at depth of 46 feet on rock. Drilled to depth of 49 feet o confirm presence of rock.			
 50 - <u>- 5.0</u>					49.0 Bottom of borehole at 49.0 feet. Borehole backfilled with drill cuttings and 3.5 bags of gravel. Ground surface restored with asphalt cold patch.			

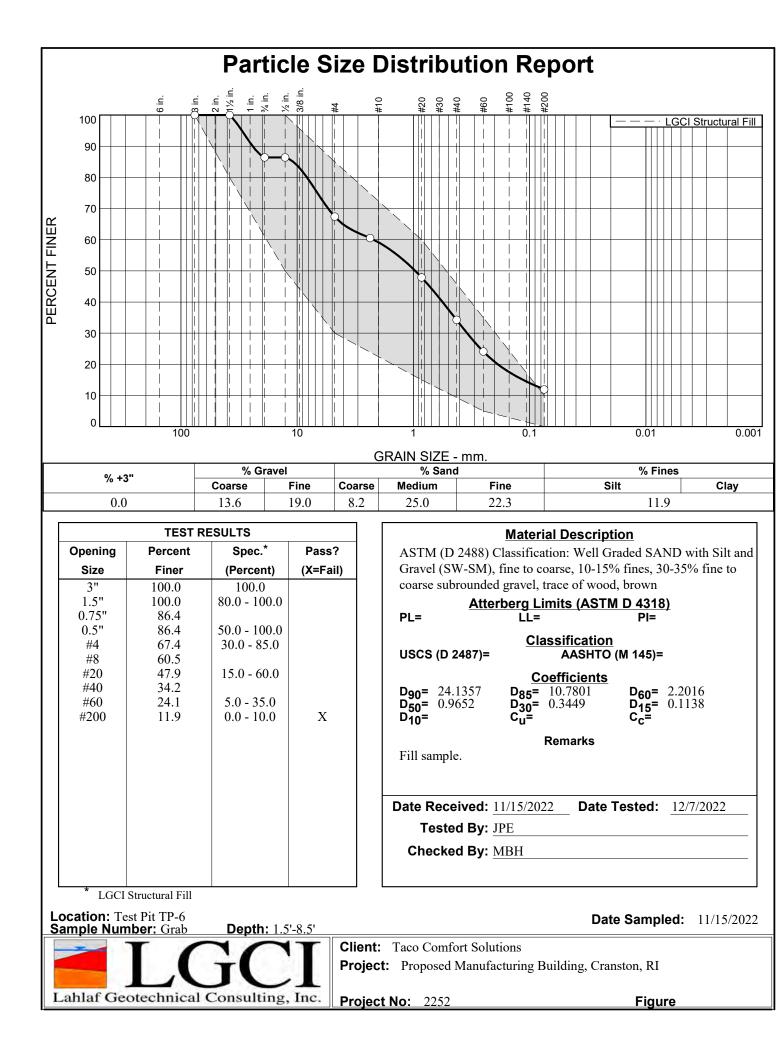
Appendix C – Laboratory Test Results

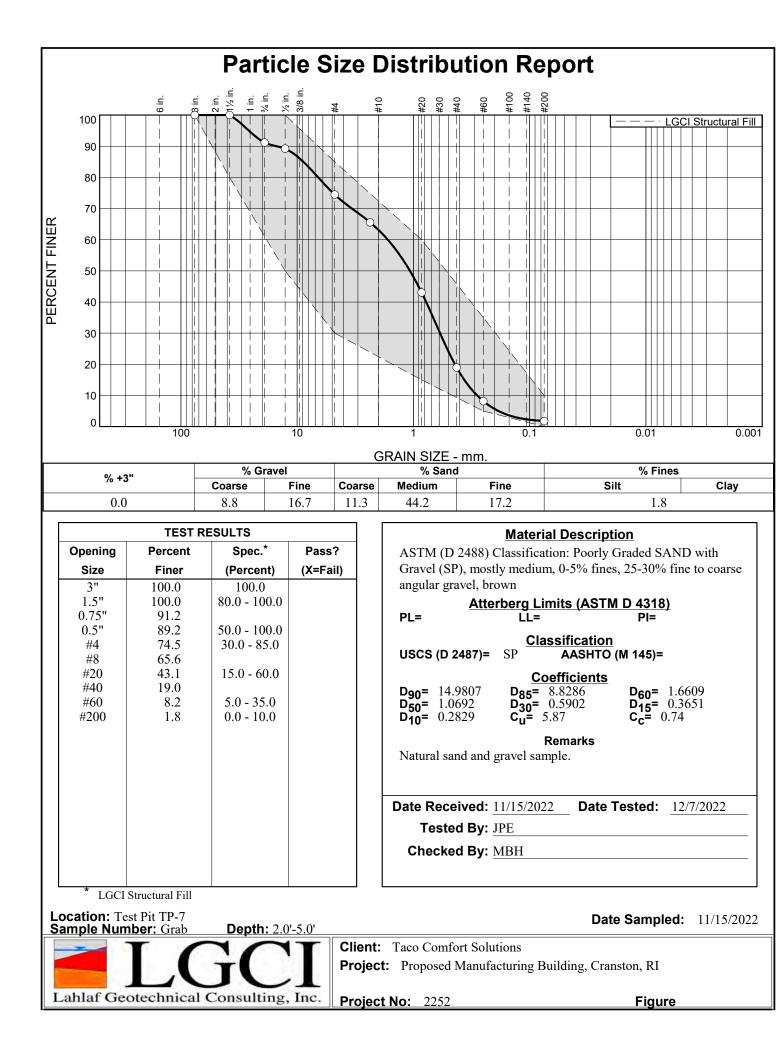


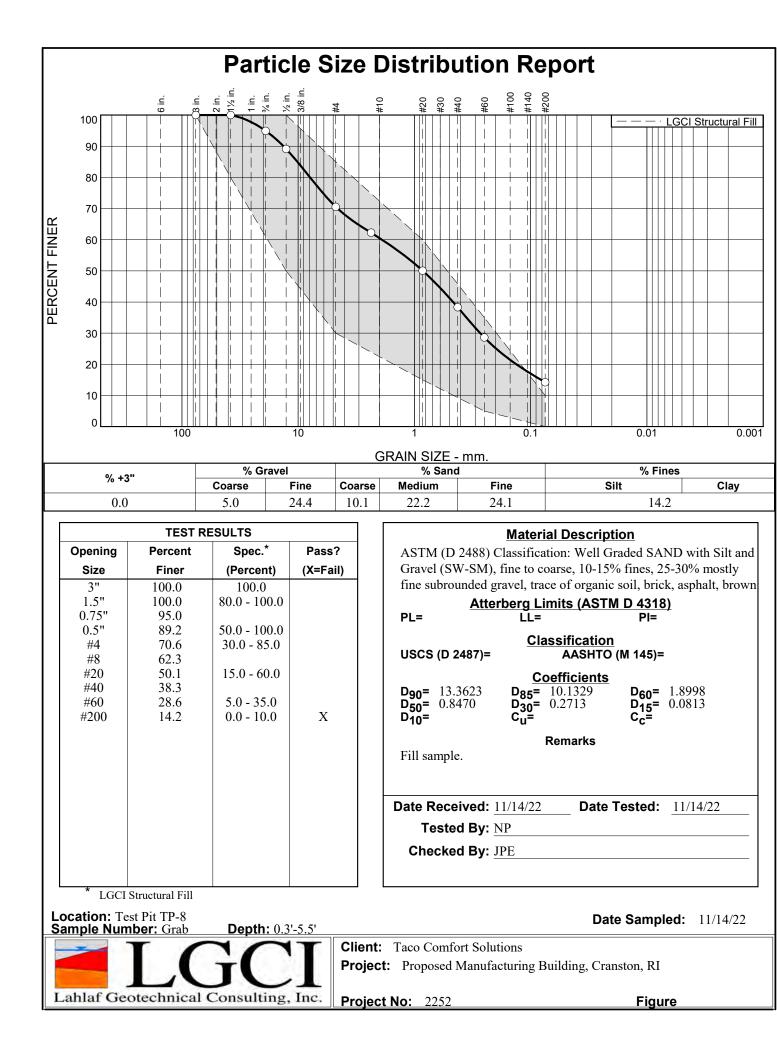


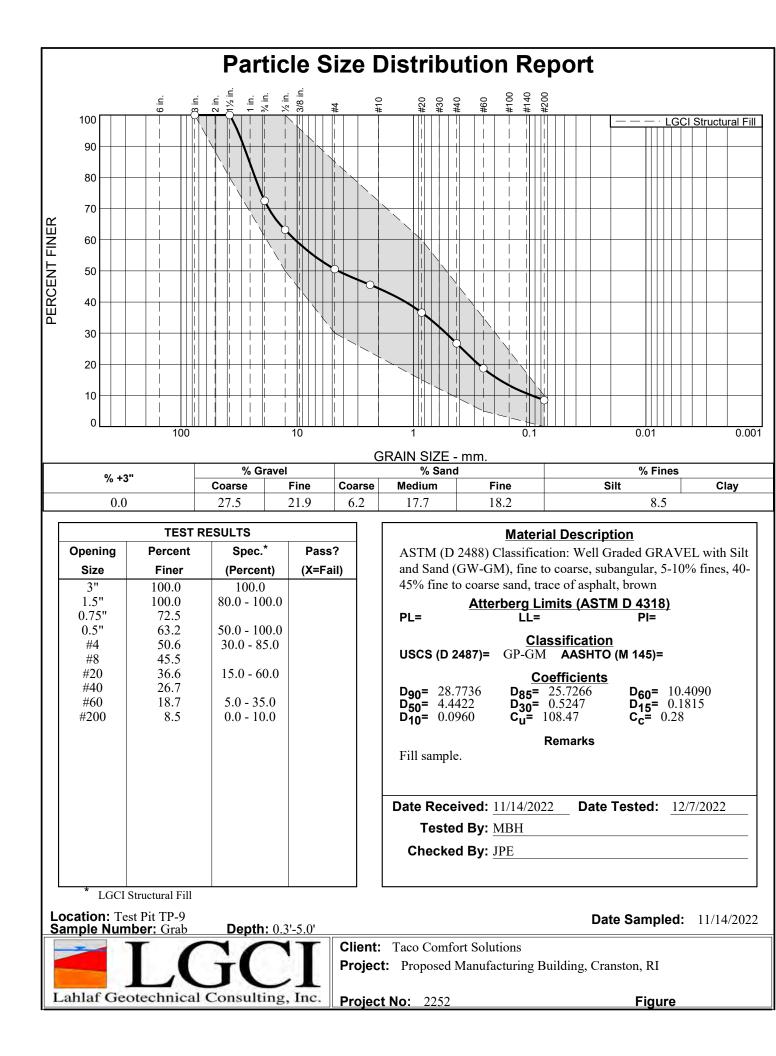














Client:	Lahlaf Geotechnical Consulting							
Project:	Prop. Manufacturing Bldg	9						
Location:	Cranston, RI			Project No:	GTX-316439			
Boring ID:		Sample Type:		Tested By:	ckg			
Sample ID	:	Test Date:	12/05/22	Checked By:	ank			
Depth :		Test Id:	696832					

Moisture, Ash, and Organic Matter - ASTM D2974

Boring ID	Sample ID	Depth	Description	Moisture Content,%	Ash Content,%	Organic Matter,%
TP-13	Fill	0.3-5	Moist, dark brown sand with gravel	11	97.8	2.2
TP-3	Fill	0.3-4	Moist, dark brown sand with gravel	6	97.4	2.6

Notes: Moisture content determined by Method A and reported as a percentage of oven-dried mass; dried to a constant mass at temperature of 105° C Ash content and organic matter determined by Method C; dried to constant mass at temperature 440° C